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Gomi et al.

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(54) **ROBOT**

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U.S.C. 154(b) by 0 days.

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Related U.S. Application Data

Primary Examiner — Ronnie Mancho

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(30) **Foreign Application Priority Data**

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(57) **ABSTRACT**

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B25J 9/16 (2006.01)

(52) **U.S. Cl.**

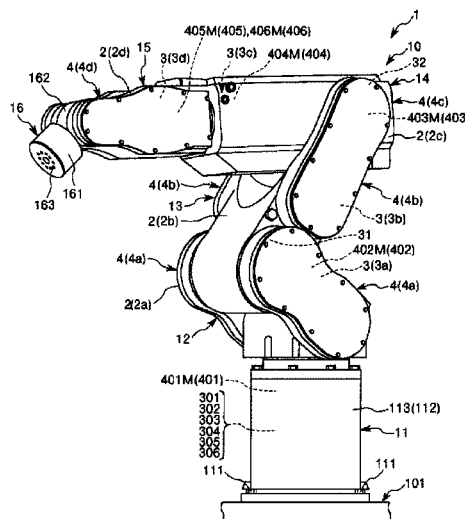
CPC **B25J 9/1638** (2013.01); **B25J 9/1651**
(2013.01); **B25J 9/1694** (2013.01); **G05B**
2219/39195 (2013.01); **G05B 2219/39335**
(2013.01); **G05B 2219/40597** (2013.01)

(58) **Field of Classification Search**

USPC 700/258, 250, 259, 245; 901/1, 14, 15,
901/19, 27, 46; 318/568.1, 568.23, 567
See application file for complete search history.

A robot includes a base, first and second arms, first and second drive sources, first and second inertia sensors, and first and second angle sensors. A rotation axis of the first arm and a rotation axis of the second arm are orthogonal to each other. The first inertia sensor is installed at the first arm, and the second inertia sensor is installed at the second arm. The first angle sensor is installed at the first drive source, and the second angle sensor is installed at the second drive source. Angular velocities obtained from the first inertia sensor and the first angle sensor are fed back to a first drive source control unit. Angular velocities obtained from the second inertia sensor and the second angle sensor are fed back to a second drive source control unit.

7 Claims, 14 Drawing Sheets



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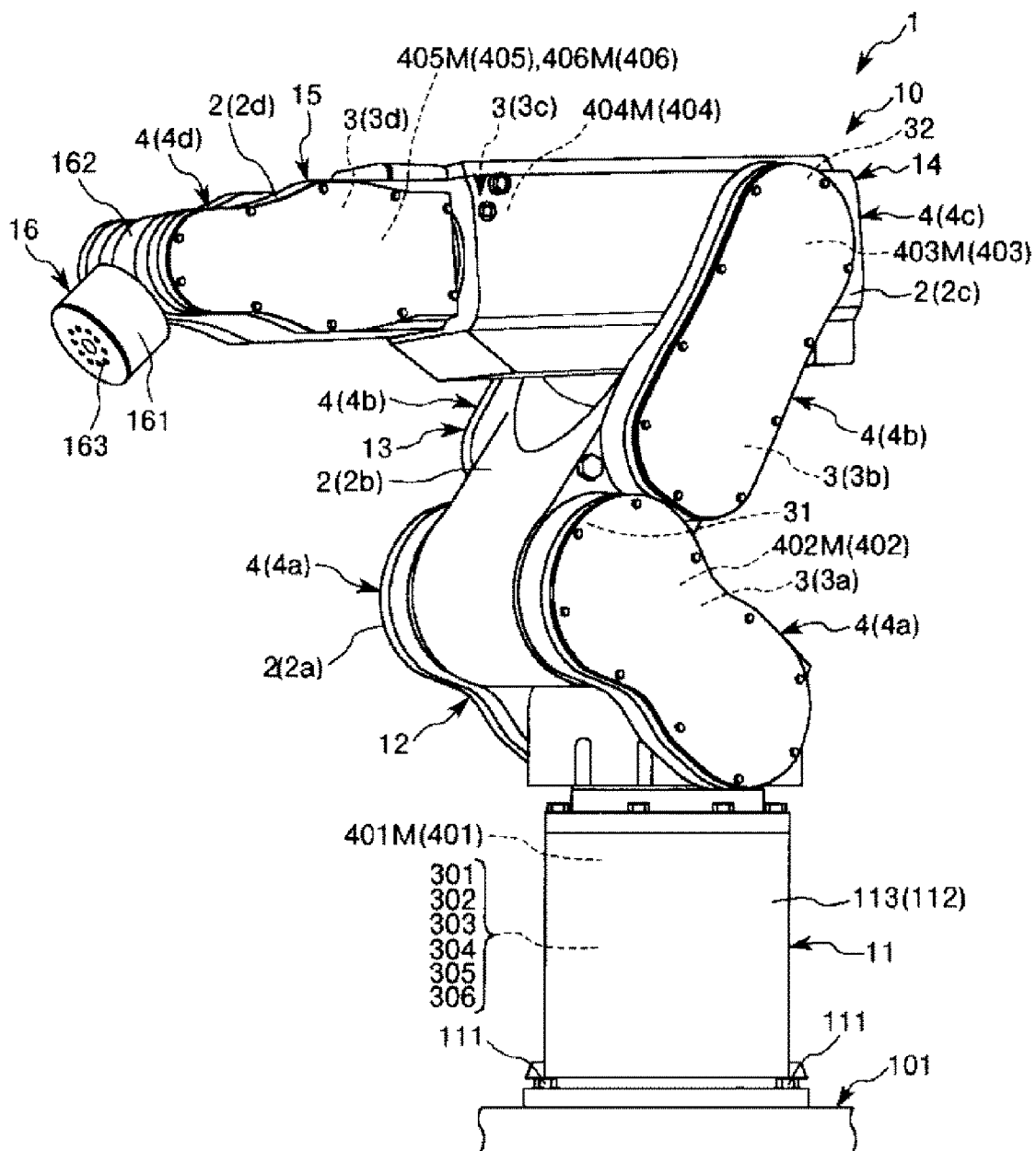


FIG. 1

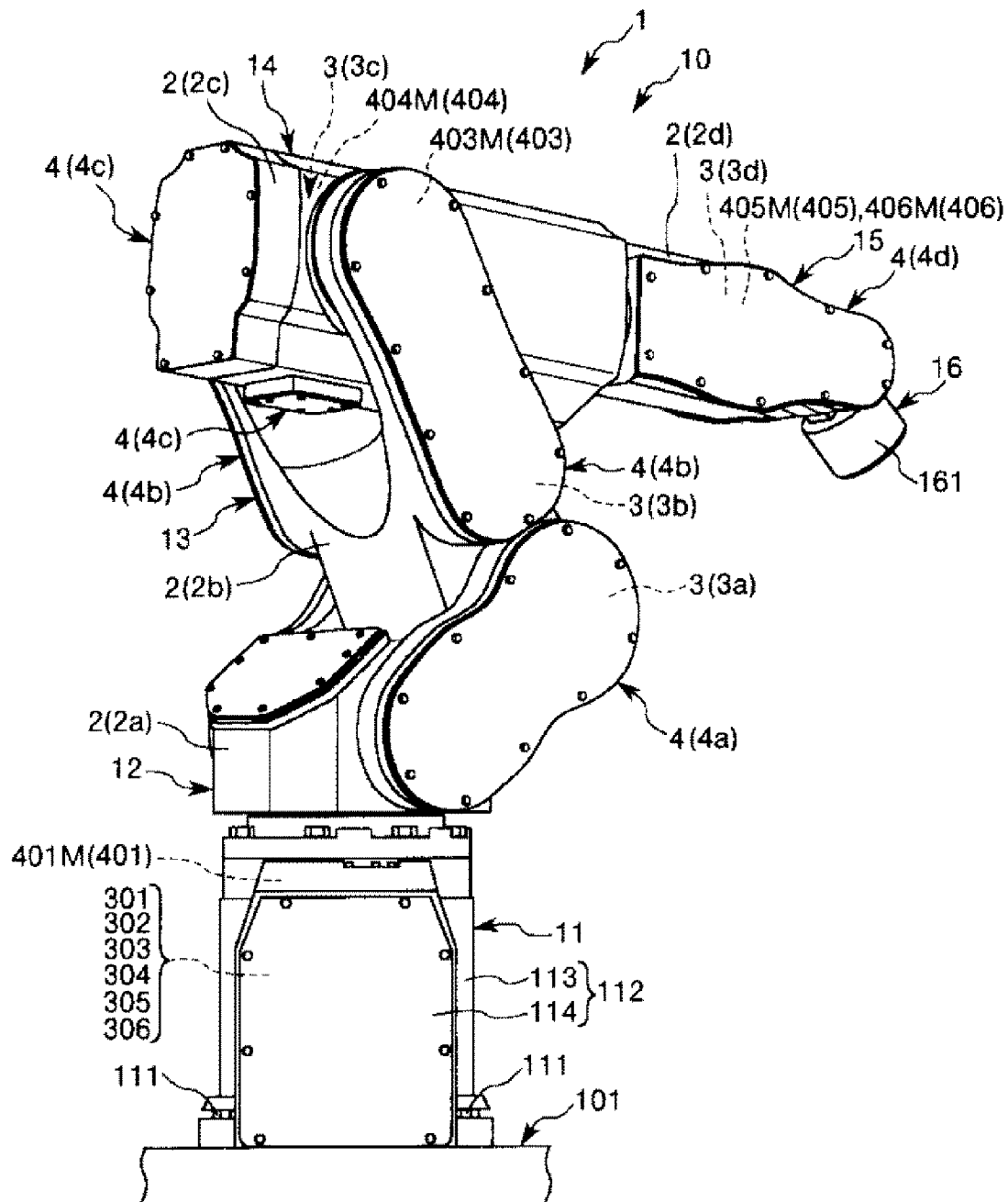


FIG. 2

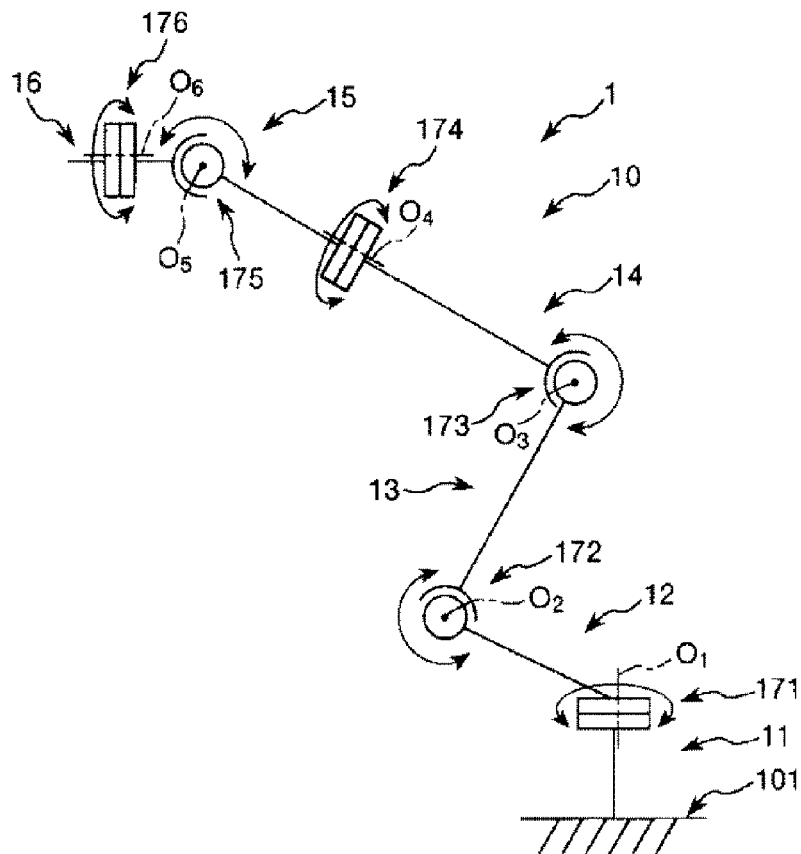


FIG. 3

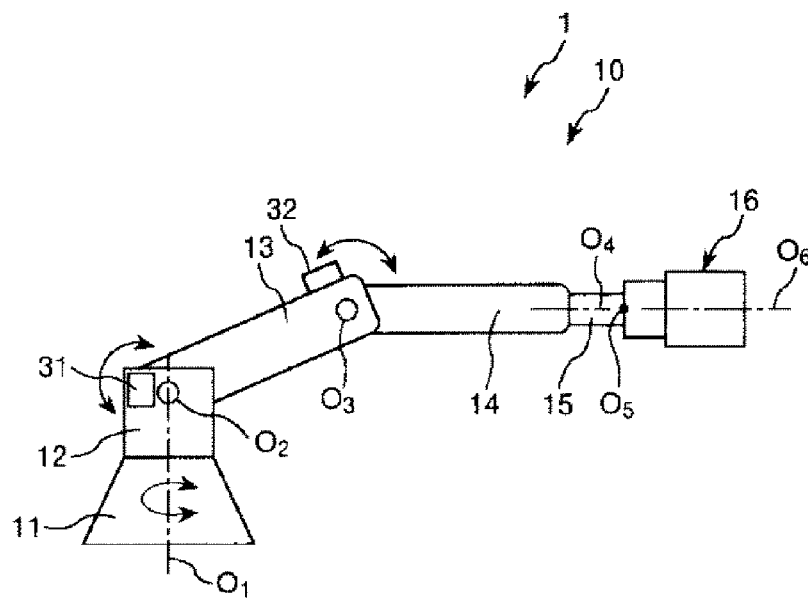


FIG. 4

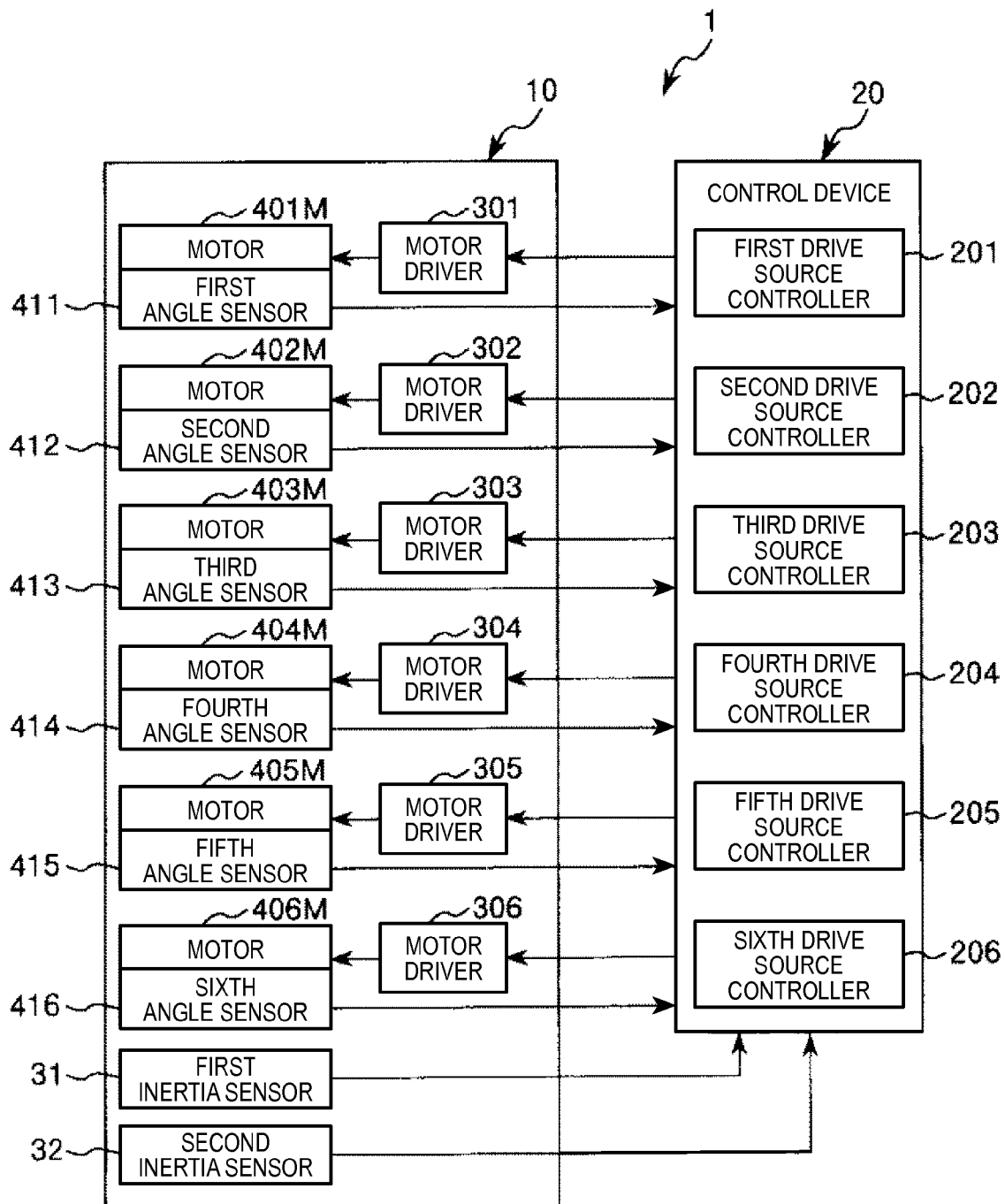


FIG. 5

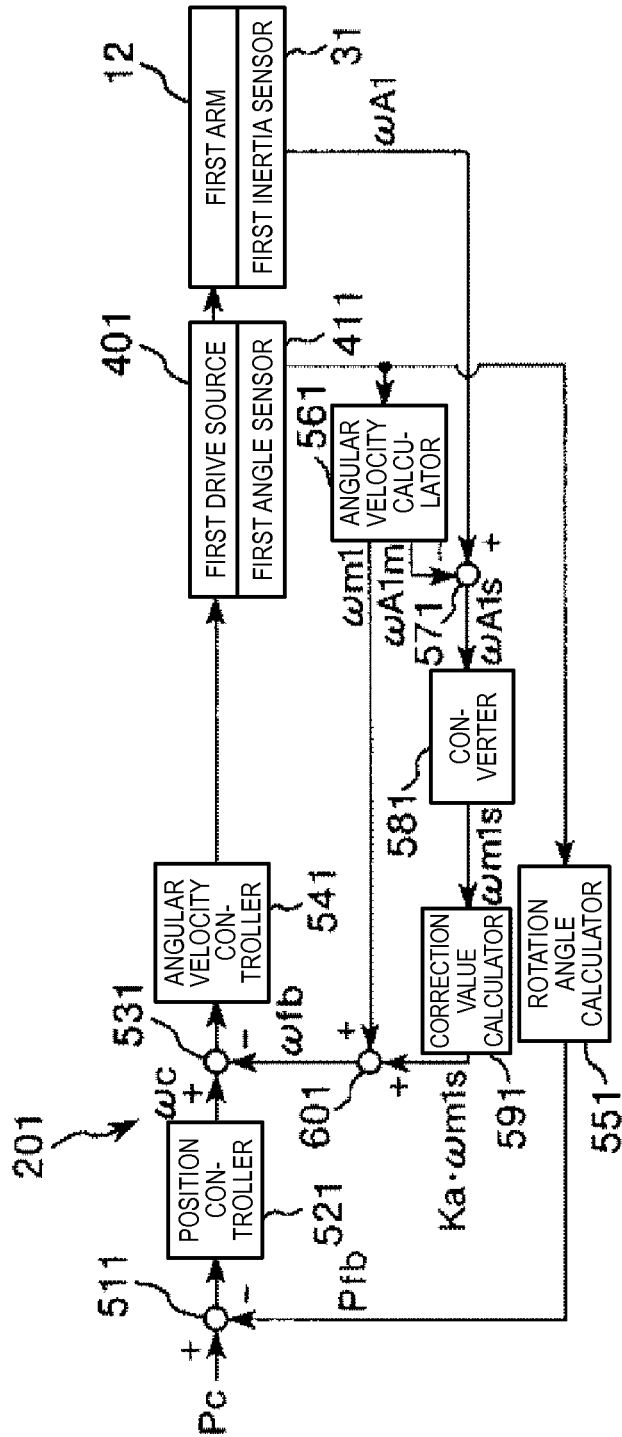


FIG. 6

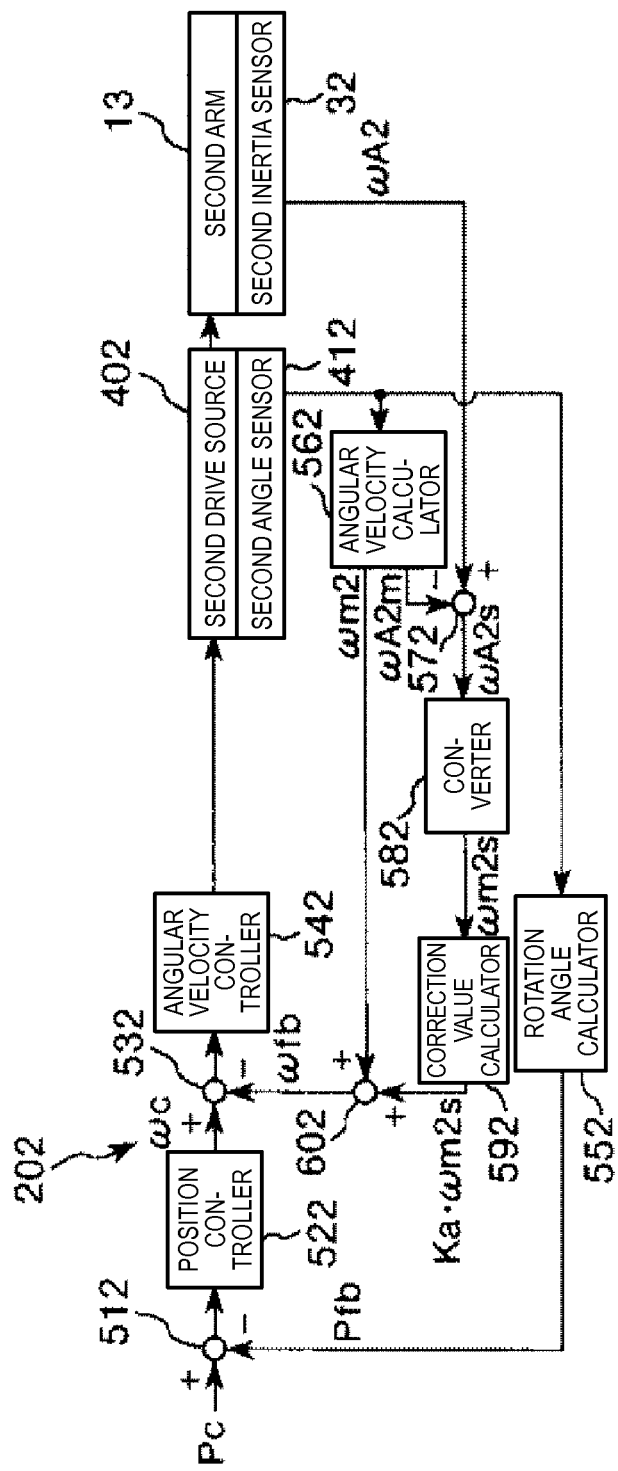


FIG. 7

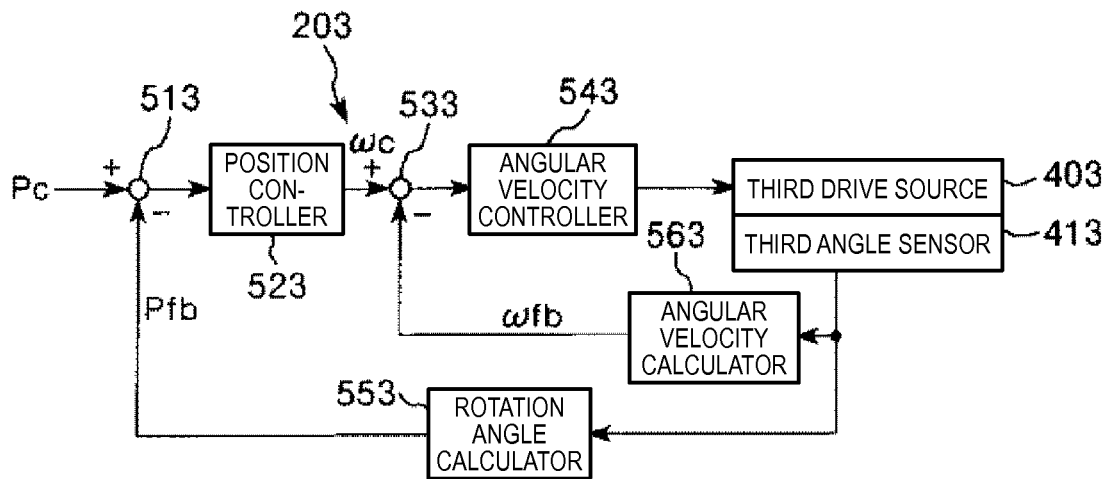


FIG. 8

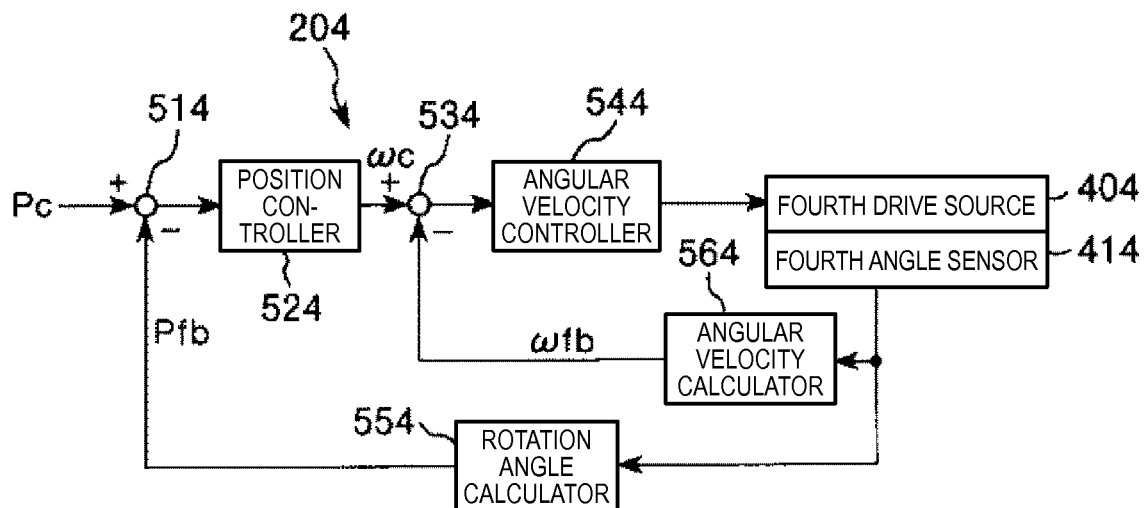


FIG. 9

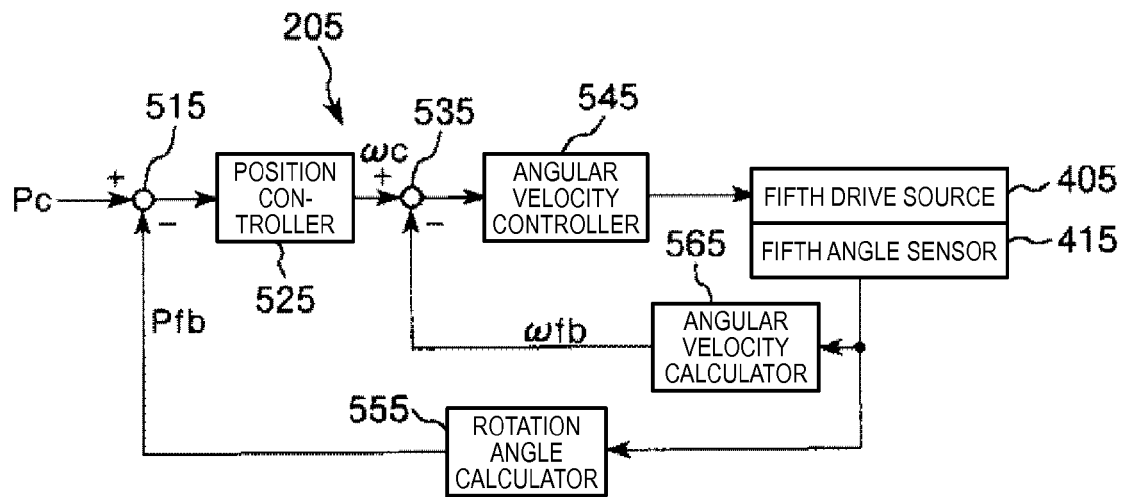


FIG.10

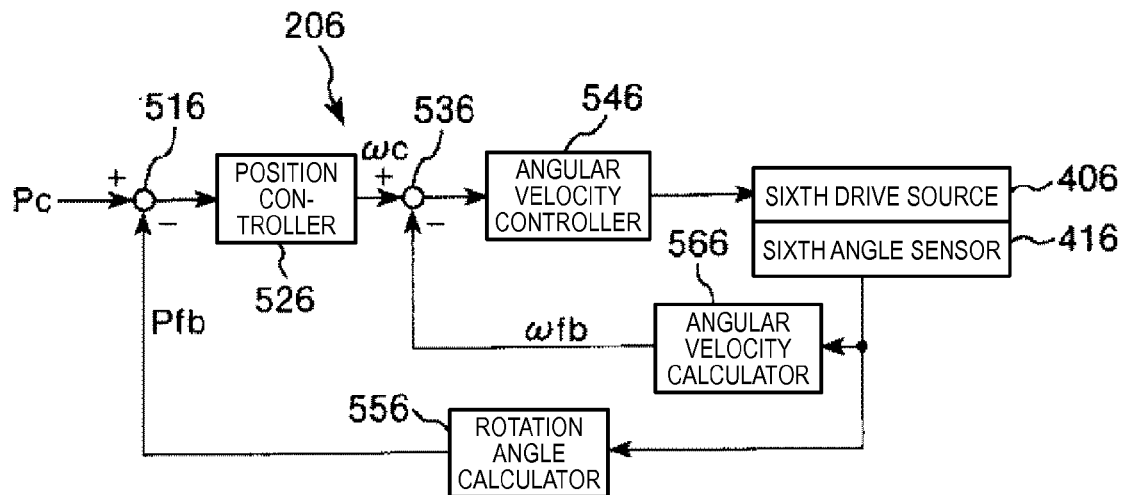


FIG.11

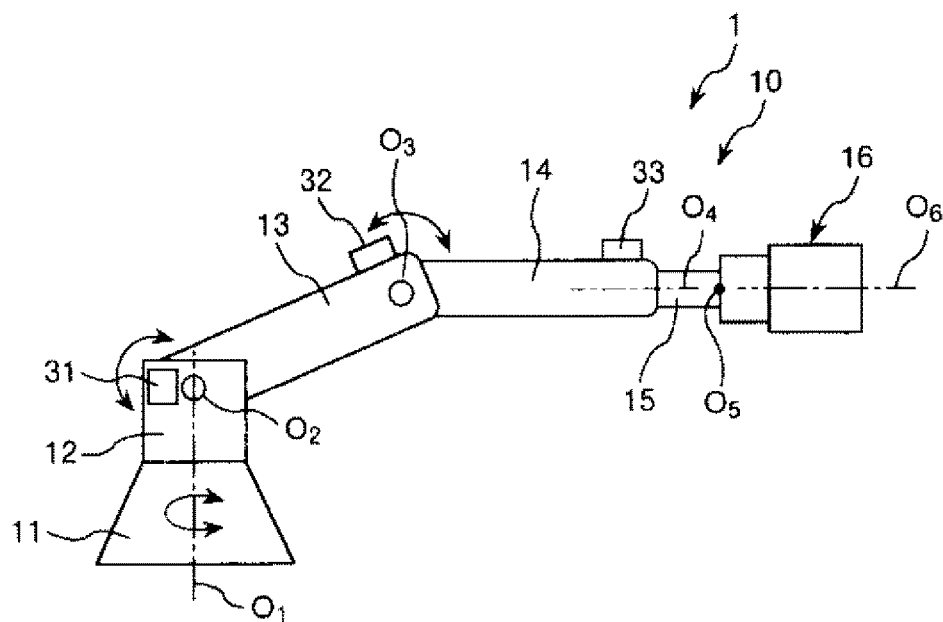


FIG.12

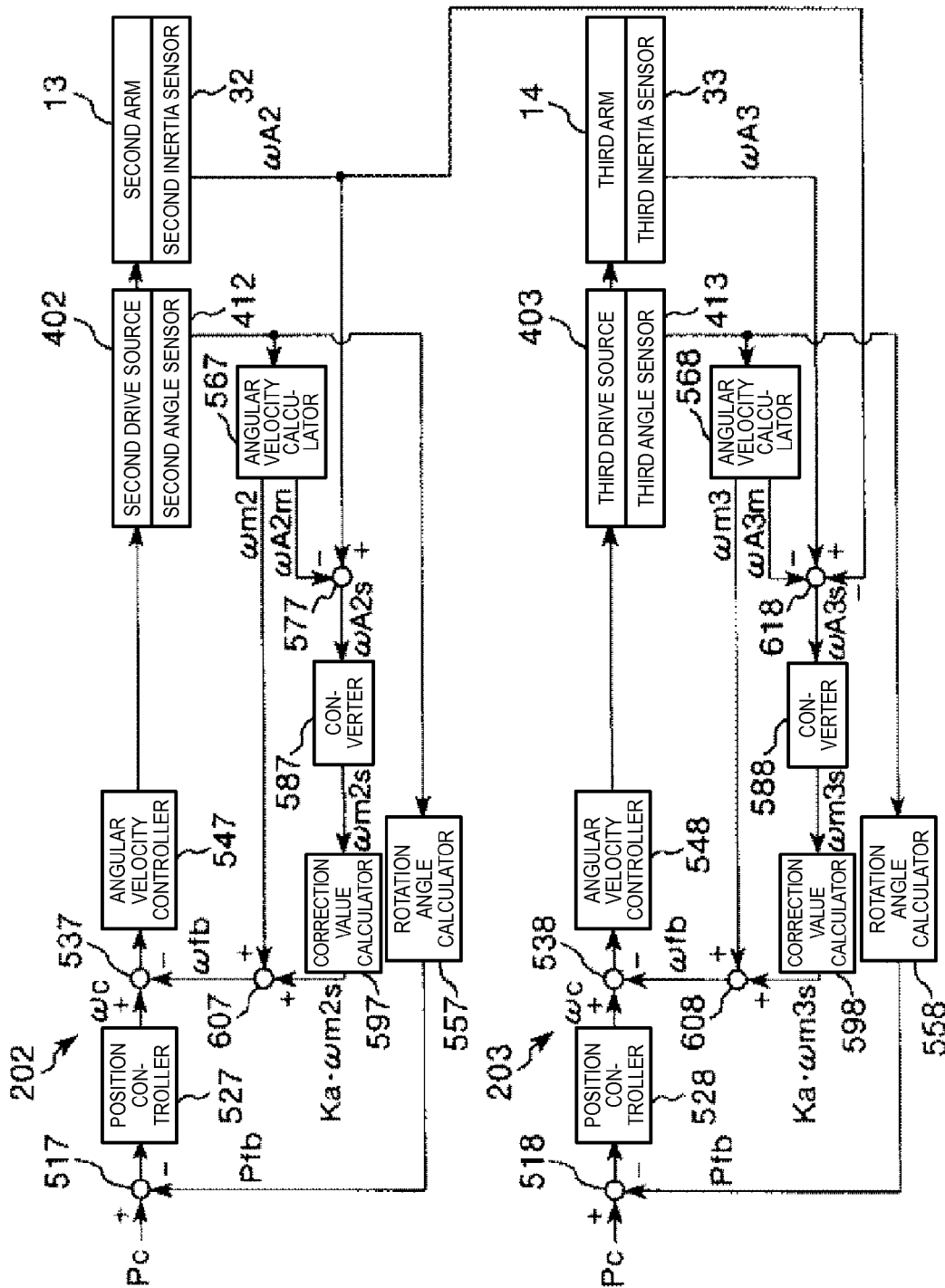


FIG.13

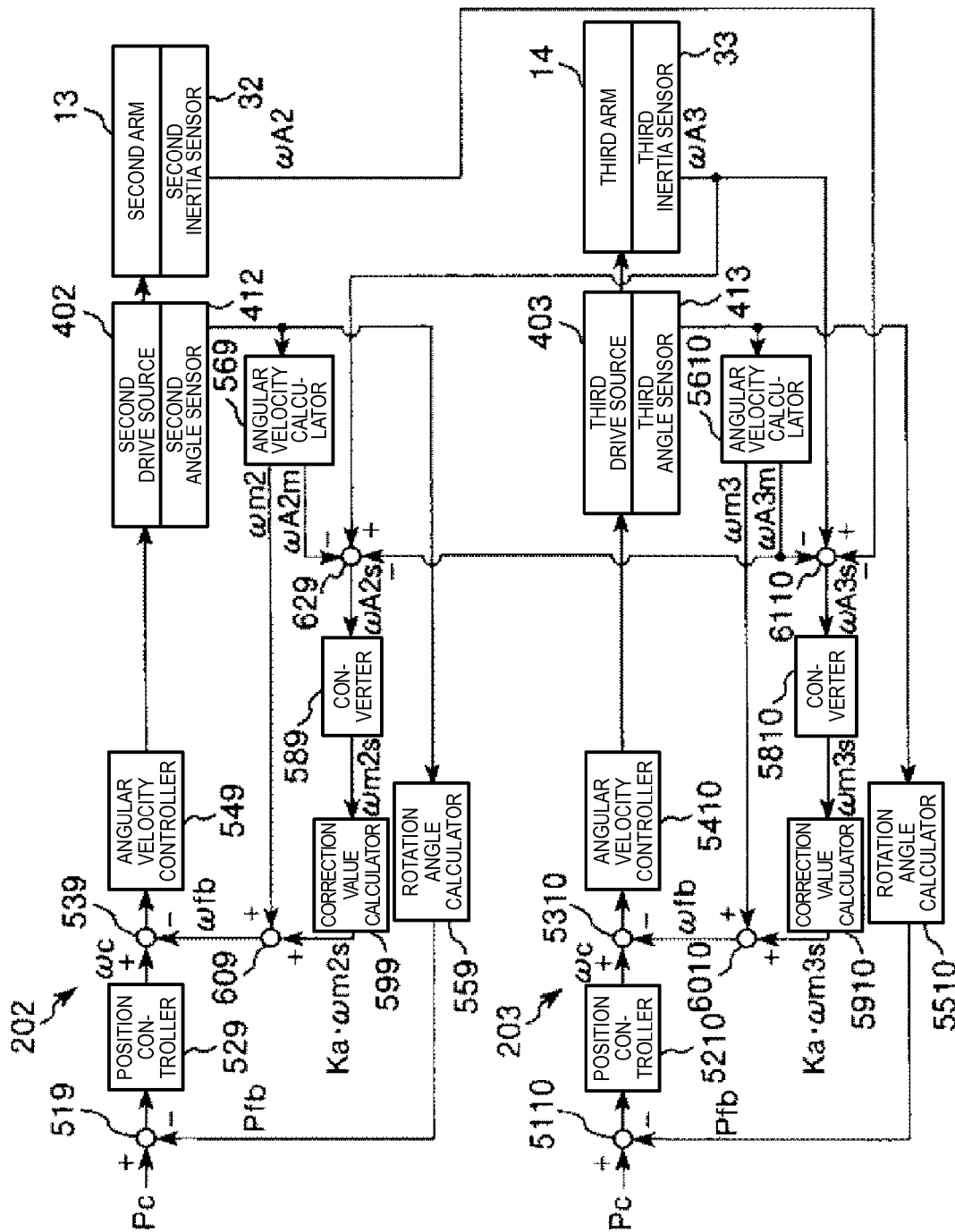


FIG.14

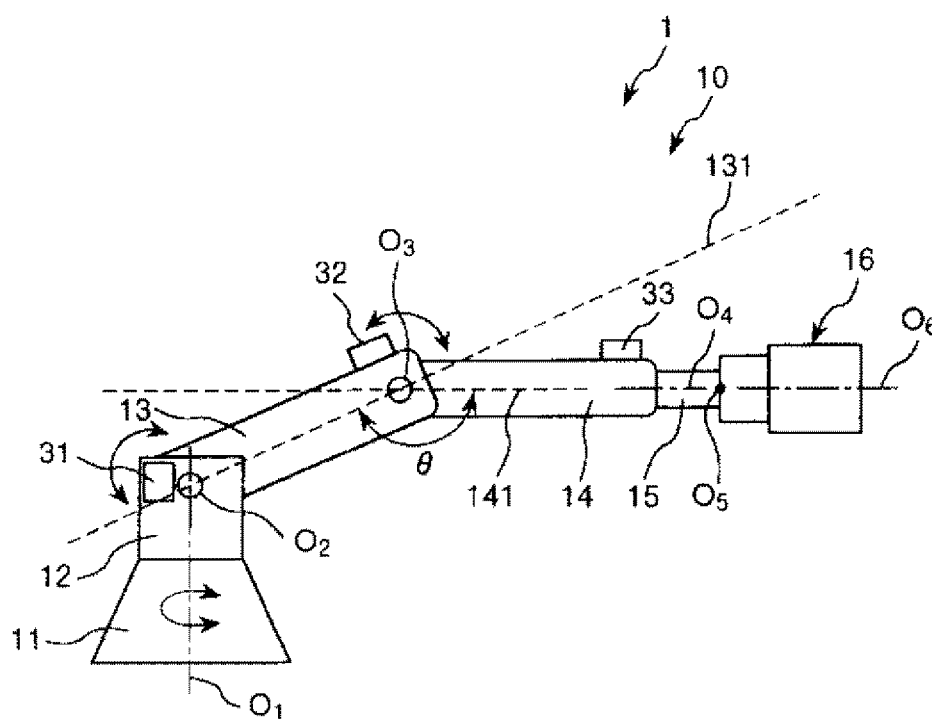


FIG.15

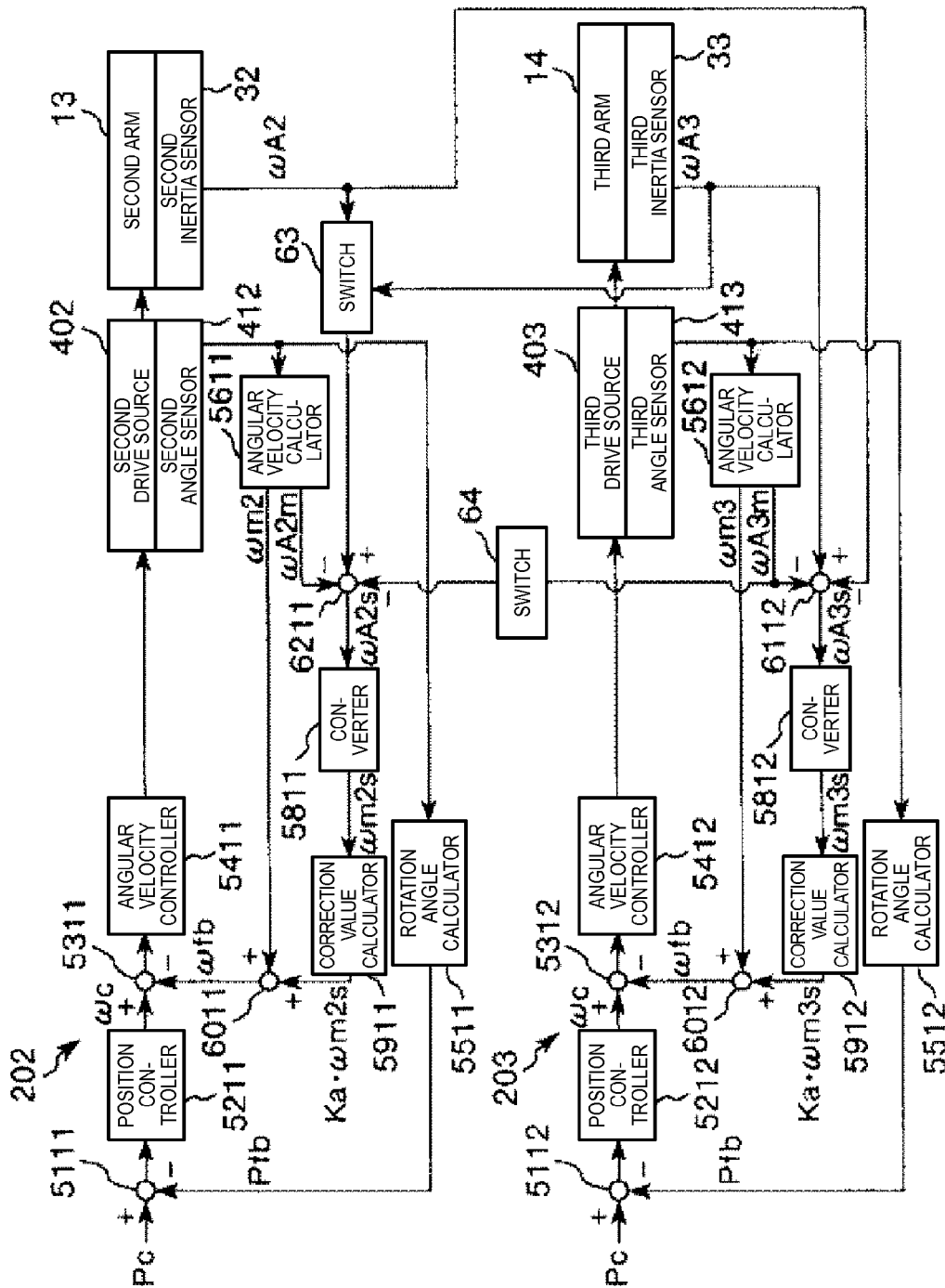


FIG. 16

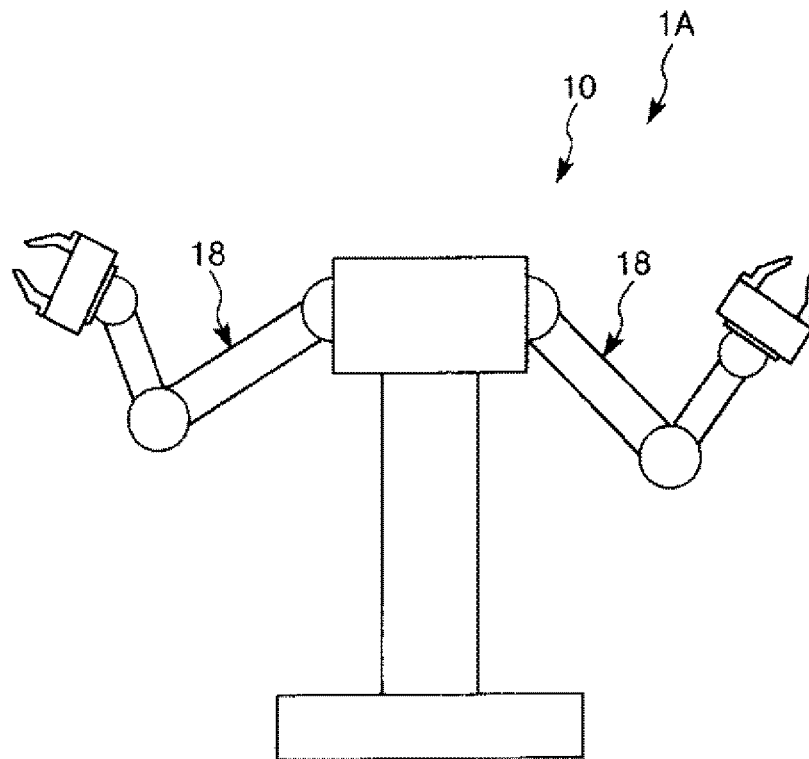


FIG.17

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ROBOT**CROSS-REFERENCE TO RELATED APPLICATIONS**

This is a continuation patent application of U.S. application Ser. No. 14/015,075 filed Aug. 30, 2013, which claims priority to Japanese Patent Application No. 2012-191449 filed Aug. 31, 2012, both of which are expressly incorporated by reference herein in their entireties.

BACKGROUND**1. Technical Field**

The present invention relates to a robot.

2. Related Art

A multi-axis robot that includes a base and a plurality of rotatable arms and that works freely in a three-dimensional space has a problem in that vibration is easily generated in the arms due to the rotation of the arms or the disturbance applied to the arms. For the purpose of attenuating the problems of vibration, a known robot includes a vibration suppressing control technique using acceleration sensors that are provided on an arm closest to the tip side and detect acceleration in the directions of three axes including the X-axis, the Y-axis, and the Z-axis (for example, refer to JP-A-10-100085). Another known multi-axis robot includes a base and a plurality of arms and has the rotation axes of the arms parallel to each other and provides angular velocity sensors on the arms, respectively, and is controlled by calculations that also include the components detected using the angular velocity sensors (for example, refer to JP-A-2005-242794).

However, the robots described in JP-A-10-100085 and JP-A-2005-242794 have the following drawbacks.

In the robot of JP-A-10-100085, the acceleration sensor is installed at the tip portion of the arm link portion closest to the tip side. Thus, the acceleration detected by the acceleration sensor is converted and corrected into those for the respective joint portions. At this time, since it is necessary to perform a coordinate axis transformation referred to as the Jacobi's transformation, and a matrix calculation having a number of sine and cosine factors is required, the amount of calculations becomes huge. Since it is necessary to calculate the factors according to the rotation angles of the motors of the respective joint portions that change every moment, it is always necessary to execute huge calculations. Accordingly, there is a drawback in that the response speed becomes slow.

Additionally, since accurate acceleration or speed cannot be fed back if calculation precision declines, vibration suppression capability may decline or control performance may be impaired. For this reason, there is a restriction on the design of a control system such that a high-speed computing unit is required, for example.

Additionally, in the calculation of the coordinate axis transformation, there is a region (incalculable region) with no coordinate axis transformation solution referred to as a singular point. In this region, the vibration suppression capability may decline or vibration may be increased instead.

In the robot of JP-A-2005-242794, since the rotation axes of the arms are parallel to each other and the directions of the components detected by the angular velocity sensors are the same, a calculation and control method in which different rotational components are mixed are not taken into consideration. Accordingly, even if this technique is adopted for a

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multi-axis robot in which the rotation axes of the arms are different from each other, vibration suppression capability cannot be satisfied.

SUMMARY

An advantage of some aspects of the disclosure is to provide a multi-axis robot that can easily and reliably suppress vibration in a robot that includes a plurality of arms and has the rotation axes of the arms different from each other.

Application Example 1

This application example is directed to a robot including a base; a first arm that is coupled to the base and rotates with a first rotation axis as an axial center; a second arm that is coupled to the first arm and rotates with a second rotation axis in a direction orthogonal to the first rotation axis as an axial center; a first drive source that rotates the first arm through a first angular velocity command; a first inertia sensor that is installed at the first arm and detects the angular velocity or acceleration of the first rotation axis of the first arm; a first angle sensor that detects the rotation angle of the first drive source; a second drive source that rotates the second arm through a second angular velocity command; a second inertia sensor that is installed at the second arm and detects the angular velocity or acceleration of the second rotation axis of the second arm; a second angle sensor that detects the rotation angle of the second drive source; a first drive source control unit that feeds back a first correction component, which is derived from an angular velocity $\omega A1$ of the first rotation axis of the first arm obtained from the first inertia sensor and an angular velocity $\omega A1m$ of the first rotation axis of the first arm obtained from the first angle sensor, and controls the first drive source; and a second drive source control unit that feeds back a second correction component, which is derived from an angular velocity $\omega A2$ of the second rotation axis of the second arm obtained from the second inertia sensor, and an angular velocity $\omega A2m$ of the second rotation axis of the second arm obtained from the second angle sensor, and controls the second drive source.

With this configuration, the vibration in the robot can be easily and reliably suppressed.

That is, a huge calculation is unnecessary, and thereby, the response speed in the control of the robot can be increased. Additionally, since a calculation in which a singular point is present is unnecessary, the control of the robot can be reliably performed, and vibration can be reliably suppressed.

Additionally, since the inertia sensors are installed at the first arm and the second arm, respectively, and the rotation axis for the rotation of the first arm and the rotation axis for the rotation of the second arm are made orthogonal to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Hence, since control is performed by the calculation using these velocities, the vibration in the robot can be more easily, accurately, and reliably suppressed.

Application Example 2

In the robot of the application example, it is preferable that the robot further includes the first drive source control unit that feeds back the first angular velocity command by the first correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A1m$ from the angular velocity $\omega A1$, by a feedback gain; and the second drive source control unit that feeds back the second angular

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velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ from the angular velocity $\omega A2$, by a feedback gain.

With this configuration, the vibration in the robot can be more reliably suppressed. In addition, since the rotation axis for the rotation of the first arm and the rotation axis for the rotation of the second arm are made orthogonal to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Since the rotational components with no mixture of these velocities are multiplied by feedback gains, respectively, the respective rotational components can be corrected with high precision. Hence, since control is performed by the calculation using these velocities, the vibration in the robot can be more easily, accurately, and reliably suppressed.

Application Example 3

This application example is directed to a robot including a base; a first arm that is coupled to the base and rotates with a first rotation axis as an axial center; a second arm that is coupled to the first arm and rotates with a second rotation axis in a direction orthogonal to the first rotation axis as an axial center; a third arm that rotates with a third rotation axis in a direction parallel to the second rotation axis as an axial center; a first drive source that rotates the first arm through a first angular velocity command; a first inertia sensor that is installed at the first arm and detects the angular velocity or acceleration of the first rotation axis of the first arm; a first angle sensor that detects the rotation angle of the first drive source; a second drive source that rotates the second arm through a second angular velocity command; a second inertia sensor that is installed at the second arm and detects the angular velocity or acceleration of the second rotation axis of the second arm; a second angle sensor that detects the rotation angle of the second drive source; a third drive source that rotates the third arm through a third angular velocity command; a third inertia sensor that is installed at the third arm and detects the angular velocity or acceleration of the second rotation axis of the third arm; a third angle sensor that detects the rotation angle of the third drive source; a first drive source control unit that feeds back a first correction component, which is derived from an angular velocity $\omega A1$ of the first rotation axis of the first arm obtained from the first inertia sensor and an angular velocity $\omega A1m$ of the first rotation axis of the first arm obtained from the first angle sensor, and controls the first drive source; a second drive source control unit that feeds back a second correction component, which is derived from an angular velocity $\omega A2$ of the second rotation axis of the second arm obtained from the second inertia sensor, an angular velocity $\omega A2m$ of the second rotation axis of the second arm obtained from the second angle sensor, and controls the second drive source; and a third drive source control unit that feeds back a third correction component, which is derived from the angular velocity $\omega A2$, an angular velocity $\omega A3$ of the second rotation axis of the third arm obtained from the third inertia sensor, and an angular velocity $\omega A3m$ of the third rotation axis of the third arm obtained from the third angle sensor, and controls the third drive source.

With this configuration, the vibration in the robot can be easily and reliably suppressed.

That is, a huge calculation is unnecessary, and thereby, the response speed in the control of the robot can be increased. Additionally, since a calculation in which a singular point is present is unnecessary, the control of the robot can be reliably performed, and vibration can be reliably suppressed.

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Additionally, since the inertia sensors are installed at the respective arms and the control of suppressing the vibration is performed on the respective arms, the vibration in the robot can be more reliably suppressed.

Additionally, since the inertia sensors are installed at the first arm, the second arm, and the third arm, respectively, and the rotation axis for the rotation of the first arm and the rotation axis for the rotation of the second arm are made orthogonal to each other, and the rotation axis for the rotation of the second arm and the rotational axis for the rotation of the third arm are made parallel to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Hence, since control is performed by the calculation using these velocities, the vibration in the robot can be more easily, accurately, and reliably suppressed.

Application Example 4

In the robot of the application example, it is preferable that the robot further includes the first drive source control unit that feeds back the first angular velocity command by the first correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A1m$ from the angular velocity $\omega A1$, by a feedback gain; the second drive source control unit that feeds back the second angular velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ from the angular velocity $\omega A2$, by a feedback gain; and the third drive source control unit that feeds back the third angular velocity command by the third correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain.

With this configuration, the vibration in the robot can be more reliably suppressed. In addition, since the rotation axis for the rotation of the first arm and the rotation axis for the rotation of the second arm are made orthogonal to each other and the rotation axis for the rotation of the second arm and the rotational axis for the rotation of the third arm are made parallel to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Since the rotational components with no mixture of these velocities are multiplied by feedback gains, respectively, the respective rotational components can be corrected with high precision. Hence, since control is performed by the calculation using these velocities, the vibration in the robot can be more easily, accurately, and reliably suppressed.

Application Example 5

This application example is directed to a robot including a base; a first arm that is coupled to the base and rotates with a first rotation axis as an axial center; a second arm that is coupled to the first arm and rotates with a second rotation axis in a direction orthogonal to the first rotation axis as an axial center; a third arm that rotates with a third rotation axis in a direction parallel to the second rotation axis as an axial center; a first drive source that rotates the first arm through a first angular velocity command; a first inertia sensor that is installed at the first arm and detects the angular velocity or acceleration of the first rotation axis of the first arm; a first angle sensor that detects the rotation angle of the first drive source; a second drive source that rotates the second arm through a second angular velocity command; a second inertia

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sensor that is installed at the second arm and detects the angular velocity or acceleration of the second rotation axis of the second arm; a second angle sensor that detects the rotation angle of the second drive source; a third drive source that rotates the third arm through a third angular velocity command; a third inertia sensor that is installed at the third arm and detects the angular velocity or acceleration of the second rotation axis of the third arm; a third angle sensor that detects the rotation angle of the third drive source; a first drive source control unit that feeds back a first correction component, which is derived from an angular velocity $\omega A1$ of the first rotation axis of the first arm obtained from the first inertia sensor and an angular velocity $\omega A1m$ of the first rotation axis of the first arm obtained from the first angle sensor, and controls the first drive source; a second drive source control unit that feeds back a second correction component, which is derived from an angular velocity $\omega A3$ of the second rotation axis of the third arm obtained from the third inertia sensor, an angular velocity $\omega A2m$ of the second rotation axis of the second arm obtained from the second angle sensor, and an angular velocity $\omega A3m$ of the third rotation axis of the third arm obtained from the third angle sensor, and controls the second drive source; and a third drive source control unit that feeds back a third correction component, which is derived from an angular velocity $\omega A2$ of the second rotation axis of the second arm obtained from the second inertia sensor, the angular velocity $\omega A3$, and the angular velocity $\omega A3m$, and controls the third drive source.

With this configuration, the vibration in the robot can be easily and reliably suppressed.

That is, a huge calculation is unnecessary, and thereby, the response speed in the control of the robot can be increased. Additionally, since a calculation in which a singular point is present is unnecessary, the control of the robot can be reliably performed, and vibration can be reliably suppressed.

Additionally, since the inertia sensors are installed at the respective arms and the control of suppressing the vibration is performed on the respective arms, the vibration in the robot can be more reliably suppressed.

Particularly, since the second drive source control unit performs the control of suppressing vibration on the second drive source that controls the operation of the second drive source, that is, rotates the second arm by the angular velocities $\omega A3$, $\omega A2m$, and $\omega A3m$, using the detection result of the third inertia sensor installed at the third arm where a larger vibration than the second arm is generated, the effect of suppressing the vibration can be enhanced.

Application Example 6

In the robot of the application example, it is preferable that the robot further includes the first drive source control unit that feeds back the first angular velocity command by the first correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A1m$ from the angular velocity $\omega A1$, by a feedback gain; the second drive source control unit that feeds back the second angular velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain; and the third drive source control unit that feeds back the third angular velocity command by the third correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain.

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Accordingly, the vibration in the robot can be more reliably suppressed. In addition, since the rotation axis for the rotation of the first arm and the rotation axis for the rotation of the second arm are made orthogonal to each other and the rotation axis for the rotation of the second arm and the rotational axis for the rotation of the third arm are made parallel to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Since the rotational components with no mixture of these velocities are multiplied by feedback gains, respectively, the respective rotational components can be corrected with high precision. Hence, since control is performed by the calculation using these velocities, the vibration in the robot can be more easily, accurately, and reliably suppressed. Particularly, in the second drive source control unit, a value including a component detected by the third inertia sensor is multiplied by a feedback gain. Thus, the effect of suppressing vibration can be further enhanced.

Application Example 7

This application example is directed to a robot including a base; a first arm that is coupled to the base and rotates with a first rotation axis as an axial center; a second arm that is coupled to the first arm and rotates with a second rotation axis in a direction orthogonal to the first rotation axis as an axial center; a third arm that rotates with a third rotation axis in a direction parallel to the second rotation axis as an axial center; a first drive source that rotates the first arm through a first angular velocity command; a first inertia sensor that is installed at the first arm and detects the angular velocity or acceleration of the first rotation axis of the first arm; a first angle sensor that detects the rotation angle of the first drive source; a second drive source that rotates the second arm through a second angular velocity command; a second inertia sensor that is installed at the second arm and detects the angular velocity or acceleration of the second rotation axis of the second arm; a second angle sensor that detects the rotation angle of the second drive source; a third drive source that rotates the third arm through a third angular velocity command; a third inertia sensor that is installed at the third arm and detects the angular velocity or acceleration of the second rotation axis of the third arm; a third angle sensor that detects the rotation angle of the third drive source; an angle detection unit that detects that the arm angle formed between an axis of the second arm and an axis of the third arm; a first drive source control unit that feeds back a first correction component, which is derived from an angular velocity $\omega A1$ of the first rotation axis of the first arm obtained from the first inertia sensor and an angular velocity $\omega A1m$ of the first rotation axis of the first arm obtained from the first angle sensor, and controls the first drive source; a second drive source control unit that feeds back either a value which is derived from an angular velocity $\omega A3$ of the second rotation axis of the third arm obtained from the third inertia sensor, an angular velocity $\omega A2m$ of the second rotation axis of the second arm obtained from the second angle sensor, and an angular velocity $\omega A3m$ of the third rotation axis of the third arm obtained from the third angle sensor, or a value which is derived from an angular velocity $\omega A2$ of the second rotation axis of the second arm obtained from the second inertia sensor, and the angular velocity $\omega A2m$, as a second correction component according to the arm angle, and controls the second drive source; and a third drive source control unit that feeds back a third correction component, which is derived from the angular velocity $\omega A2$, the angular velocity $\omega A3$, and the angular velocity $\omega A3m$, and controls the third drive source.

With this configuration, the vibration in the robot can be easily and reliably suppressed.

That is, a huge calculation is unnecessary, and thereby, the response speed in the control of the robot can be increased. Additionally, since a calculation in which a singular point is present is unnecessary, the control of the robot can be reliably performed, and vibration can be reliably suppressed.

Additionally, since the inertia sensors are installed at the respective arms and the control of suppressing the vibration is performed on the respective arms, the vibration in the robot can be more reliably suppressed.

Particularly, since the second drive source control unit selects and feeds back either a value derived from the angular velocity $\omega A3$, the angular velocity $\omega A2m$, and the angular velocity $\omega A3m$ or a value derived from the angular velocity $\omega A2$ and the angular velocity $\omega A2m$ on the basis of the detection results of the angle detection unit, the compatibility between the effect of suppressing vibration and the stability of control can be achieved.

Application Example 8

In the robot of the application example, it is preferable that the robot further includes the first drive source control unit that feeds back the first angular velocity command by the first correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A1m$ from the angular velocity $\omega A1$, by a feedback gain; the second drive source control unit that feeds back the second angular velocity command, using either a value obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain, or a value obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ from the angular velocity $\omega A2$, by a feedback gain, as the second correction component; and the third drive source control unit that feeds back the third angular velocity command by the third correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain.

With this configuration, the vibration in the robot can be more reliably suppressed.

Application Example 9

In the robot of the application example, it is preferable that the robot further includes the second drive source control unit that feeds back the second angular velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain when the arm angle is equal to or larger than a first threshold and is equal to or smaller than a second threshold that is larger than the first threshold and that feeds back the second angular velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ from the angular velocity $\omega A2$, by a feedback gain when the arm angle is smaller than the first threshold or larger than the second threshold.

Accordingly, the compatibility between enhancing the effect of suppressing vibration and the stability of control can be more reliably achieved.

That is, when the angle θ formed between the axis of the second arm and the axis of the third arm is equal to or larger than the first threshold and equal to or smaller than the second

threshold (extended posture), the control of the robot is stable but the inertia moment of the robot is large and the vibration in the robot is large, compared to a case (folded posture) where the angle θ formed between the axis of the second arm and the axis of the third arm is smaller than the first threshold or larger than the second threshold. Thus, the effect of suppressing vibration can be enhanced by feeding back the second angular velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ and the angular velocity $\omega A3m$ from the angular velocity $\omega A3$, by a feedback gain.

That is, when the angle θ formed between the axis of the second arm and the axis of the third arm is smaller than the first threshold or larger than the second threshold, the inertia moment of the robot is small and the vibration in the robot is small but control tends to become unstable and the robot vibrates easily, compared to a case where the angle θ formed between the axis of the second arm and the axis of the third arm is equal to or larger than the first threshold and equal to or smaller than the second threshold. Thus, the vibration in the robot can be prevented and control can be stabilized, by feeding back the second angular velocity command by the second correction component obtained by multiplying a value, which is obtained by subtracting the angular velocity $\omega A2m$ from the angular velocity $\omega A2$, by a feedback gain.

Application Example 10

In the robot of the application example, it is preferable that the first threshold is set within a range of 45° to 135° , and the second threshold is set within a range of 225° to 315° .

With this configuration, the compatibility between enhancing the effect of suppressing vibration and the stability of control can be more reliably achieved.

Application Example 11

In the robot of the application example, it is preferable that the first inertia sensor is installed at a tip portion in the rotation of the first arm, and the second inertia sensor is installed at a tip portion in the rotation of the second arm.

With this configuration, since the first inertia sensor detects the angular velocity or acceleration of the first arm in a region where the vibration in the first arm is at the maximum and the second inertia sensor detects the angular velocity or acceleration of the second arm in a region where the vibration in the second arm is at the maximum, the vibration in the robot can be more reliably suppressed.

Application Example 12

In the robot of the application examples, it is preferable that the first inertia sensor is installed at a tip portion in the rotation of the first arm, the second inertia sensor is installed at a tip portion in the rotation of the second arm, and the third inertia sensor is installed at a tip portion in the rotation of the third arm.

With this configuration, since the first inertia sensor detects the angular velocity or acceleration of the first arm in a region where the vibration in the first arm is at the maximum, the second inertia sensor detects the angular velocity or acceleration of the second arm in a region where the vibration in the second arm is at the maximum, and the third inertia sensor detects the angular velocity or acceleration of the third arm in a region where the vibration in the third arm is at the maximum, the vibration in the robot can be more reliably suppressed.

Application Example 13

In the robot of the application example, it is preferable that the first rotation axis coincides with the normal line of an installation surface of the base.

With this configuration, the robot can be easily controlled.

Application Example 14

This application example is directed to a robot including a base; a first arm that is coupled to the base and rotates with a first rotation axis as an axial center; a second arm that rotates with a second rotation axis orthogonal to the first rotation axis as an axial center; a first inertia sensor that detects the angular velocity of the first arm; a first angle sensor that detects the rotation angle of a drive source of the first arm; a second inertia sensor that detects the angular velocity of the second arm; a second angle sensor that detects the rotation angle of a drive source of the second arm; a control unit of the drive source of the first arm that feeds back an angular velocity derived from a detection result of the first angle sensor and an angular velocity detected from the first inertia sensor; and a control unit of the drive source of the second arm that feeds back an angular velocity derived from a detection result of the second angle sensor and an angular velocity detected from the second inertia sensor.

With this configuration, it is possible to provide a multi-joint robot that can freely work in a three-dimensional space but easily and reliably suppresses vibration caused by driving.

In the robot of the application example, since the arms are coupled so that the rotation axes orthogonal to each other or the rotation axes parallel to each other are mixed, information from one inertia sensor may be only information on at least one coordinate axis. Accordingly, for example, coordinate axis transformation, such as the Jacobi's transformation, is unnecessary, and feedback to the controller can be performed using a simple calculation.

That is, a calculation for performing feedback to the controller on the basis of huge information is unnecessary, and thereby, the response speed in the control of the robot can be increased. Additionally, since a calculation in which a singular point is present is unnecessary, the control of the robot can be reliably performed, and vibration can be reliably suppressed. In addition, although the control unit of the drive source of the first arm and the control unit of the drive source of the second arm are built on mutually independent calculation circuits, the control units can be built on the same IC circuit.

Application Example 15

This application example is directed to a robot including a plurality of orthogonal rotation axes, one inertia sensor and one angle sensor are provided so as to correspond to each of the orthogonal rotation axes, and angular velocities obtained from the angle sensor and the inertia sensor are feedback-controlled for every rotation axis corresponding to the angle sensor and the inertia sensor.

With this configuration, it is possible to provide a multi-joint robot that can freely work in a three-dimensional space but easily and reliably suppresses vibration caused by driving.

Since the robot of the application example includes a plurality of orthogonal rotation axes, one inertia sensor and one angle sensor are provided so as to correspond to each of the orthogonal rotation axes, and angular velocities obtained

from the angle sensor and the inertia sensor are feedback-controlled for every rotation axis corresponding to the angle sensor and the inertia sensor, information from the inertia sensor may be only information on at least one coordinate axis. Accordingly, for example, coordinate axis transformation, such as the Jacobi's transformation, is unnecessary, and feedback to the controller can be performed using a simple calculation.

That is, a calculation for performing feedback to the controller on the basis of huge information is unnecessary, and thereby, the response speed in the control of the robot can be increased. Additionally, since a calculation in which a singular point is present is unnecessary, the control of the robot can be reliably performed, and vibration can be reliably suppressed. In addition, when one inertia sensor and one angle sensor may be provided so as to correspond to every orthogonal rotation axis, and a plurality of parallel rotation axes are present, one rotation axis of them may be selected from a rotation axis orthogonal to the one rotation axis, and one inertia sensor and one angle sensor may be provided for these rotation axes, respectively.

BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the invention will be described with reference to the accompanying drawings, wherein like numbers reference like elements.

FIG. 1 is the perspective view when a first embodiment of a robot is viewed from the front side.

FIG. 2 is a perspective view when the robot shown in FIG. 1 is viewed from the back side.

FIG. 3 is a schematic view of the robot shown in FIG. 1.

FIG. 4 is a schematic view of the robot shown in FIG. 1.

FIG. 5 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 6 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 7 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 8 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 9 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 10 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 11 is a block diagram of portions of the robot shown in FIG. 1.

FIG. 12 is a schematic view showing a second embodiment of a robot.

FIG. 13 is a block diagram of portions of the robot shown in FIG. 12.

FIG. 14 is a block diagram showing portions of a third embodiment of a robot.

FIG. 15 is a schematic view showing a fourth embodiment of a robot.

FIG. 16 is a block diagram of portions of the robot shown in FIG. 15.

FIG. 17 is a front view showing another configuration example of a robot.

DESCRIPTION OF EXEMPLARY EMBODIMENTS

A robot will be described below in detail on the basis of preferred embodiments shown in the accompanying drawings.

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First Embodiment

FIG. 1 is the perspective view when a first embodiment of a robot is viewed from the front side. FIG. 2 is a perspective view when the robot shown in FIG. 1 is viewed from the back side. FIGS. 3 and 4 are schematic views of the robot shown in FIG. 1, respectively. FIG. 5 is a block diagram of portions of the robot shown in FIG. 1, and FIGS. 6 to 11 are block diagrams of portions of the robot shown in FIG. 1, respectively.

In addition, in the following, for convenience of description, the upper side in FIGS. 1 to 4 is referred to as “upper” or “upside” and the lower side is referred to as “lower” or “downside”. Additionally, the base side in FIGS. 1 to 4 is referred to as a “base end”, and the opposite side is referred to as a “tip”. Additionally, the rotation axes O2 and O3 are shown in an exaggerated manner in FIG. 4, respectively. Additionally, inertia sensors 31 and 32 are shown outside arms 12 and 13 in FIG. 4, respectively, in order to clarify the presence of the sensors.

A robot (industrial robot) 1 shown in FIGS. 1 to 4 can be used for, for example, a manufacturing process that manufactures precision mechanical equipment, such as a wrist watch, and has a robot body 10 and a control device (control unit) 20 (refer to FIG. 5) that controls the operation of the robot body 10. The robot body 10 and the control device 20 are electrically connected. Additionally, the control device 20 can be constituted by, for example, a personal computer (PC) in which a central processing unit (CPU) is built. In addition, the control device 20 is described below in more detail.

The robot body 10 includes a base 11, four arms (links) 12, 13, 14, and 15, a wrist (link) 16, and six drive sources 401, 402, 403, 404, 405, and 406. The robot body 10 is a vertical multi-joint (six-axis) robot (robot body) in which the base 11, the arms 12, 13, 14, and 15, and the wrist 16 are coupled together in the order from a base end side toward a tip side. In the vertical multi-joint robot, the base 11, the arms 12 to 15, and the wrist 16 can also be collectively referred to as “arms”, and the arm 12, the arm 13, the arm 14, the arm 15, and the wrist 16 can be referred to as a “first arm”, a “second arm”, a “third arm”, a “fourth arm”, and a “fifth or sixth arm”, respectively. In addition, the wrist 16 may have the fifth arm and the sixth arm. An end effector or the like can be attached to the wrist 16.

As shown in FIGS. 3 and 4, the arms 12 to 15 and the wrist 16 are supported so as to be independently displaceable with respect to the base 11. The lengths of the arms 12 to 15 and the wrist 16 are not particularly limited, respectively. However, in the illustrated configuration, the lengths of the arms 12 to 14 are set to be larger than those of the other arm 15 and the wrist 16. In addition, for example, the length of the third arm 14 may be made smaller than the lengths of the first arm 12 and the second arm 13.

The base 11 and the first arm 12 are coupled together via a joint 171. The first arm 12 has a first rotation axis O1 parallel to the vertical direction as a rotation center, and is rotatable with respect to the base 11 around the first rotation axis O1. The first rotation axis O1 coincides with the normal line of an upper surface of a floor 101 that is an installation surface of the base 11. The rotation around the first rotation axis O1 is performed by the driving of the first drive source 401. Additionally, the first drive source 401 is driven by a motor 401M and a cable (not shown), and the motor 401M is controlled by the control device 20 via a motor driver 301 that is electrically connected thereto (refer to FIG. 5). The driving from the motor 401M may be transmitted to the first drive source 401

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by a speed reducer (not shown) provided together with the motor 401M, and the speed reducer may be omitted.

The first arm 12 and the second arm 13 are coupled together via a joint 172. The second arm 13 is rotatable with respect to the first arm 12 with the second rotation axis O2 parallel to the horizontal direction as an axial center. The second rotation axis O2 is orthogonal to the first rotation axis O1. The rotation around the second rotation axis O2 is performed by the driving of the second drive source 402. Additionally, the second drive source 402 is driven by a motor 402M and a cable (not shown), and the motor 402M is controlled by the control device 20 via a motor driver 302 that is electrically connected thereto (refer to FIG. 5). The driving from the motor 402M may be transmitted to the second drive source 402 by a speed reducer (not shown) provided in addition to the motor 402M, and the speed reducer may be omitted.

The second arm 13 and the third arm 14 are coupled together via a joint 173. The third arm 14 has a rotation axis O3 parallel to the horizontal direction as a rotation center, and is rotatable with respect to the second arm 13 around the third rotation axis O3. The third rotation axis O3 is parallel to the second rotation axis O2. The rotation around the third rotation axis O3 is performed by the driving of the third drive source 403. Additionally, the third drive source 403 is driven by a motor 403M and a cable (not shown), and the motor 403M is controlled by the control device 20 via a motor driver 303 that is electrically connected thereto (refer to FIG. 5). The driving from the motor 403M may be transmitted to the third drive source 403 by a speed reducer (not shown) provided in addition to the motor 403M, and the speed reducer may be omitted.

The third arm 14 and the fourth arm 15 are coupled together via a joint 174. The fourth arm 15 has a fourth rotation axis O4 parallel to the direction of a central axis of the third arm 14 as a rotation center, and is rotatable with respect to the third arm 14 (base 11) around the fourth rotation axis O4. The fourth rotation axis O4 is orthogonal to the third rotation axis O3. The rotation around the fourth rotation axis O4 is performed by the driving of the fourth drive source 404. Additionally, the fourth drive source 404 is driven by a motor 404M and a cable (not shown), and the motor 404M is controlled by the control device 20 via a motor driver 304 that is electrically connected thereto (refer to FIG. 5). The driving from the motor 404M may be transmitted to the fourth drive source 404 by a speed reducer (not shown) provided together with the motor 404M, and the speed reducer may be omitted. In addition, the fourth rotation axis O4 may be parallel to an axis orthogonal to the third rotation axis O3.

The fourth arm 15 and the wrist 16 are coupled together via a joint 175. The wrist 16 has a fifth rotation axis O5 parallel to the horizontal direction (y-axis direction) as a rotation center, and is rotatable with respect to the fourth arm 15 around the fifth rotation axis O5. The fifth rotation axis O5 is orthogonal to the fourth rotation axis O4. The rotation around the fifth rotation axis O5 is performed by the driving of the fifth drive source 405. Additionally, the fifth drive source 405 is driven by a motor 405M and a cable (not shown), and the motor 405M is controlled by the control device 20 via a motor driver 305 that is electrically connected thereto (refer to FIG. 5). The driving from the motor 405M may be transmitted to the fifth drive source 405 by a speed reducer (not shown) provided together with the motor 405M, and the speed reducer may be omitted. Additionally, the wrist 16 has a sixth rotation axis O6 vertical to the fifth rotation axis O5 as a rotation center, and is also rotatable via a joint 176 around the sixth rotation axis O6. The rotation axis O6 is orthogonal to the rotation axis O5. The rotation around the sixth rotation axis O6 is performed by the

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driving of the sixth drive source **406**. Additionally, the sixth drive source **406** is driven by a motor **406M** and a cable (not shown), and the motor **406M** is controlled by the control device **20** via a motor driver **306** that is electrically connected thereto (refer to FIG. 5). The driving from the motor **406M** may be transmitted to the sixth drive source **406** by a speed reducer (not shown) provided in addition to the motor **406M**, and the speed reducer may be omitted. In addition, the fifth rotation axis **O5** may be parallel to an axis orthogonal to the fourth rotation axis **O4**, and the sixth rotation axis **O6** may be parallel to an axis orthogonal to the fifth rotation axis **O5**.

Additionally, the first inertia sensor **31** is installed at the first arm **12**. The first inertia sensor **31** detects the angular velocity of the first arm **12** around the first rotation axis **O1**. Although the installation position of the first inertia sensor **31** at the first arm **12** is not particularly limited, a tip portion of the first arm **12** is preferable. In the present embodiment, the first inertia sensor **31** is installed at the tip portion inside the first arm **12**. Since the vibration in the first arm **12** becomes the maximum at the tip portion of the first arm, this can more reliably suppress the vibration in the robot **1**. In addition, it should be understood that the first inertia sensor **31** may be installed at a base end portion of the first arm **12**.

Additionally, a second inertia sensor **32** is installed at the second arm **13**. The second inertia sensor **32** detects the angular velocity of the second arm **13** around the second rotation axis **O2**. Although the installation position of the second inertia sensor **32** at the second arm **13** is not particularly limited, a tip portion of the second arm **13** is preferable. In the present embodiment, the second inertia sensor **32** is installed at the tip portion inside the second arm **13**. Since the vibration in the second arm **13** becomes the maximum at the tip portion of the second arm, this can more reliably suppress the vibration in the robot **1**. In addition, it should be understood that the second inertia sensor **32** may be installed at a base end portion of the second arm **13**.

Additionally, the first inertia sensor **31** and the second inertia sensor **32** are not particularly limited, respectively, and in the present embodiment, for example, a gyroscope sensor, an acceleration sensor, or the like can be used.

Here, in the robot **1**, in order to suppress the vibration in the first arm **12** and the second arm **13**, the first inertia sensor **31** and the second inertia sensor **32** are installed at both the first arm **12** and the second arm **13** as mentioned above, and the operation of the drive sources **401** and **402** is controlled on the basis of detection results of the first inertia sensor **31** and the second inertia sensor **32**. Accordingly, the vibration in the first arm **12** and the second arm **13** can be reliably suppressed, and thereby, the vibration in the entire robot **1** can be reliably suppressed.

A first angle sensor **411**, a second angle sensor **412**, a third angle sensor **413**, a fourth angle sensor **414**, a fifth angle sensor **415**, and a sixth angle sensor **416** are provided at respective motors or speed reducers in the drive sources **401** to **406**. Encoders, rotary encoders, or the like can be used as the angle sensors. The angle sensors **411** to **416** detect the rotation angles of rotating shafts of the motors or speed reducers of the drive sources **401** to **406**, respectively. The motors of the drive sources **401** to **406** are not particularly limited, respectively. For example, it is preferable to use servo motors, such as AC servo motors or DC servo motors. Additionally, the respective cables may be inserted through the robot body **10**, respectively.

As shown in FIG. 5, the robot body **10** is electrically connected to the control device **20**. That is, the drive sources

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401 to **406**, the angle sensors **411** to **416**, and the inertia sensors **31** and **32** are electrically connected to the control device **20**, respectively.

The control device **20** can independently operate the arms **12** to **15** and the wrist **16**, respectively, that is, can independently control the drive sources **401** to **406** via the motor drivers **301** to **306**, respectively. In the case, the control device **20** performs detection by the angle sensors **411** to **416**, the first inertia sensor **31**, and the second inertia sensor **32**, and controls the driving, for example, angular velocity, rotation angle, or the like of the drive sources **401** to **406** on the basis of the detection results, respectively. A control program is stored in advance in a recording medium built in the control device **20**.

As shown in FIG. 1 and FIG. 2, when the robot **1** is a vertical multi-joint robot, the base **11** is a portion that is located on the lowermost side of the vertical multi-joint robot and is fixed to the floor **101** of an installation space. The fixing method is not particularly limited, and for example, in the present embodiment shown in FIGS. 1 and 2, a fixing method using a plurality of bolts **111** is used. In addition, a fixing place in the installation space of the base **11** can also be the wall or ceiling of the installation space other than the floor.

The base **11** has a hollow base body (housing) **112**. The base body **112** can be separated into a cylindrical portion **113** that forms a cylindrical shape, and a box-shaped portion **114** that is integrally formed at an outer peripheral portion of the cylindrical portion **113** and forms a box shape. For example, the motor **401M** and the motor drivers **301** to **306** are stored in such a base body **112**.

The arms **12** to **15** have a hollow arm body **2**, a drive mechanism **3**, and a sealing unit **4**, respectively. In addition, in the following, for convenience of description, the arm body **2**, the drive mechanism **3**, and the sealing unit **4** of the first arm **12** may be referred to as an "arm body **2a**", a "drive mechanism **3a**", and a "sealing unit **4a**", respectively, the arm body **2**, the drive mechanism **3**, and the sealing unit **4** of the second arm **13** may be referred to as an "arm body **2b**", a "drive mechanism **3b**", and a "sealing unit **4b**", respectively, the arm body **2**, the drive mechanism **3**, and the sealing unit **4** of the third arm **14** may be referred to as an "arm body **2c**", a "drive mechanism **3c**", and a "sealing unit **4c**", respectively, and the arm body **2**, the drive mechanism **3**, and the sealing unit **4** of the fourth arm **15** may be referred to as an "arm body **2d**", a "drive mechanism **3d**", and a "sealing unit **4d**", respectively.

Additionally, the joints **171** to **176** have rotation support mechanisms (not shown), respectively. The rotation support mechanisms are a mechanism that supports one of two arms coupled to each other so as to be rotatable to the other, a mechanism that supports one of the base **11** and the first arm **12** coupled to each other so as to be rotatable to the other, and a mechanism that supports one of the fourth arm **15** and the wrist **16** coupled to each other so as to be rotatable to the other. When the fourth arm **15** and the wrist **16** that are coupled to each other are taken as an example, the rotation support mechanism can rotate the wrist **16** with respect to the fourth arm **15**. Additionally, each rotation support mechanism has a speed reducer (not shown) that reduces the rotating speed of a corresponding motor in a predetermined reduction ratio, and transmits the driving force thereof to a corresponding arm, the wrist body **161** of the wrist **16**, and a support ring **162**.

The first arm **12** is coupled to an upper end portion (tip portion) of the base **11** in a posture in which the first arm **12** inclines with respect to the horizontal direction. In the first arm **12**, the drive mechanism **3a** has the motor **402M**, and is

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stored within the arm body **2a**. Additionally, the inside of the arm body **2a** is hermetically sealed by the sealing unit **4a**.

The second arm **13** is coupled to a tip portion of the first arm **12**. In the second arm **13**, the drive mechanism **3b** has the motor **403M**, and is stored within the arm body **2b**. Additionally, the inside of the arm body **2b** is hermetically sealed by the sealing unit **4b**.

The third arm **14** is coupled to a tip portion of the second arm **13**. In the third arm **14**, the drive mechanism **3c** has the motor **404M**, and is stored within the arm body **2c**. Additionally, the inside of the arm body **2c** is hermetically sealed by the sealing unit **4c**.

The fourth arm **15** is coupled to a tip portion of the third arm **14** in parallel with the direction of a central axis thereof. In the arm **15**, the drive mechanism **3d** has the motors **405M** and **406M**, and is stored within the arm body **2d**. Additionally, the inside of the arm body **2d** is hermetically sealed by the sealing unit **4d**.

The wrist **16** is coupled to a tip portion (end portion opposite the base **11**) of the fourth arm **15**. For example, a manipulator (not shown) that grips precision mechanical equipment, such as a wrist watch, is detachably mounted on a tip portion (an end portion opposite the fourth arm **15**) of the wrist **16**. In addition, the manipulator is not particularly limited, and includes, for example, a manipulator of a configuration having a plurality of fingers. The robot **1** can convey the precision mechanical equipment by controlling the operation of the arms **12** to **15**, the wrist **16**, or the like with the precision mechanical equipment gripped by the manipulator.

The wrist **16** has the wrist body (sixth arm) **161** that forms a cylindrical shape, and the support ring (fifth arm) **162** that is configured separately from the wrist body **161**, is provided at a base end portion of the wrist body **161**, and forms a ring shape.

A tip face **163** of the wrist body **161** is a flat surface, and serves as a mounting surface on which the manipulator is mounted. Additionally, the wrist body **161** is coupled to the drive mechanism **3d** of the fourth arm **15** via the joint **176**, and is rotated around the rotation axis **O6** by the driving of the motor **406M** of the drive mechanism **3d**.

The support ring **162** is coupled to the drive mechanism **3d** of the fourth arm **15** via the joint **175**, and is rotated around the rotation axis **O5** of the entire wrist body **161** by the driving of the motor **405M** of the drive mechanism **3d**.

Next, the configuration of the control device **20** will be described with reference to FIGS. **5** and **6** to **11**.

As shown in FIGS. **5** and **6** to **11**, the control device **20** has a first drive source controller (first drive source control unit) (first angular velocity command) **201** that controls the operation of the first drive source **401**, a second drive source controller (second drive source control unit) (second angular velocity command) **202** that controls the operation of the second drive source **402**, a third drive source controller (third drive source control unit) (third angular velocity command) **203** that controls the operation of the third drive source **403**, a fourth drive source controller (fourth drive source control unit) (fourth angular velocity command) **204** that controls the operation of the fourth drive source **404**, a fifth drive source controller (fifth drive source control unit) (fifth angular velocity command) **205** that controls the operation of the fifth drive source **405**, and a sixth drive source controller (sixth drive source control unit) (sixth angular velocity command) **206** that controls the operation of the sixth drive source **406**.

As shown in FIG. **6**, the first drive source controller **201** has a subtractor **511**, a position controller **521**, a subtractor **531**, an angular velocity controller **541**, a rotation angle calculator

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551, an angular velocity calculator **561**, a subtractor **571**, a converter **581**, a correction value calculator **591**, and an adder **601**.

As shown in FIG. **7**, the second drive source controller **202** has a subtractor **512**, a position controller **522**, a subtractor **532**, an angular velocity controller **542**, a rotation angle calculator **552**, an angular velocity calculator **562**, a subtractor **572**, a converter **582**, a correction value calculator **592**, and an adder **602**.

As shown in FIG. **8**, the third drive source controller **203** has a subtractor **513**, a position controller **523**, a subtractor **533**, an angular velocity controller **543**, a rotation angle calculator **553**, and an angular velocity calculator **563**.

As shown in FIG. **9**, the fourth drive source controller **204** has a subtractor **514**, a position controller **524**, a subtractor **534**, an angular velocity controller **544**, a rotation angle calculator **554**, and an angular velocity calculator **564**.

As shown in FIG. **10**, the fifth drive source controller **205** has a subtractor **515**, a position controller **525**, a subtractor **535**, an angular velocity controller **545**, a rotation angle calculator **555**, and an angular velocity calculator **565**.

As shown in FIG. **11**, the sixth drive source controller **206** has a subtractor **516**, a position controller **526**, a subtractor **536**, an angular velocity controller **546**, a rotation angle calculator **556**, and an angular velocity calculator **566**.

Here, the control device **20** calculates a target position of the wrist **16** on the basis of the contents of processing to be performed by the robot **1**, and generates a track for moving the wrist **16** to the target position. The control device **20** measures the rotation angles of the respective drive sources **401** to **406** for every predetermined control cycle so that the wrist **16** moves along the generated track, and outputs values calculated on the basis of the measurement results to the drive source controllers **201** to **206** as position commands **Pc** of the respective drive sources **401** to **406**, respectively (refer to FIGS. **6** to **11**). In addition, although “values are input and output” or the like are written in the above and the following, this means “signals corresponding to the values are input and output”.

As shown in FIG. **6**, in addition to a position command **Pc** of the first drive source **401**, detection signals are input from the first angle sensor **411** and the first inertia sensor **31**, respectively, to the first drive source controller **201**. The first drive source controller **201** drives the first drive source **401** by feedback control using the respective detection signals so that a rotation angle (position feedback value **Pfb**) of the first drive source calculated from the detection signal of the first angle sensor **411** becomes the position command **Pc** and an angular velocity feedback value ω_{fb} to be described below becomes an angular velocity command ω_c to be described below.

That is, the position command **Pc** is input to the subtractor **511** of the first drive source controller **201**, and the position feedback value **Pfb** to be described below is input from the rotation angle calculator **551**. In the rotation angle calculator **551**, the number of pulses input from the first angle sensor **411** is counted, and the rotation angle of the first drive source **401** according to the counted value is output to the subtractor **511** as the position feedback value **Pfb**. The subtractor **511** outputs a deviation (value obtained by subtracting the position feedback value **Pfb** from a targeted value of the rotation angle of the first drive source **401**) between the position command **Pc** and the position feedback value **Pfb** to the position controller **521**.

The position controller **521** performs predetermined calculation processing using the deviation input from the subtractor **511** and a proportional gain that is a predetermined factor, and calculates the targeted value of the angular veloc-

ity of the first drive source **401** according to the deviation. The position controller **521** outputs a signal showing the targeted value (command value) of the angular velocity of the first drive source **401** to the subtractor **531** as the angular velocity command (first angular velocity command) ω_c . In addition, in the present embodiment, a proportional control (P control) is performed as the feedback control. However, the feedback control is not limited to this.

The angular velocity command ω_c and the angular velocity feedback value ω_{fb} to be described below are input to the subtractor **531**. The subtractor **531** outputs a deviation (value obtained by subtracting the angular velocity feedback value ω_{fb} from the targeted value of the angular velocity of the first drive source **401**) between the angular velocity command ω_c and the angular velocity feedback value ω_{fb} to the angular velocity controller **541**.

The angular velocity controller **541** performs predetermined calculation processing including integration, using the deviation input from the subtractor **531**, a proportional gain that is a predetermined factor, an integration gain, or the like, thereby generating a driving signal (driving current) of the first drive source **401** according to the deviation and supplying the driving signal to the motor **401M** via the motor driver **301**. In addition, in the present embodiment, the PI (proportion/integration) control is performed as the feedback control. However, the feedback control is not limited to this.

In this way, the feedback control is performed and the driving current of the first drive source **401** is controlled so that the position feedback value P_{fb} is as equal to the position command P_c as possible and the angular velocity feedback value ω_{fb} is as equal to the angular velocity command ω_c as possible.

Next, the angular velocity feedback value ω_{fb} in the first drive source controller **201** will be described.

In the angular velocity calculator **561**, an angular velocity ω_{m1} of the first drive source **401** is calculated on the basis of the frequency of a pulse signal input from the first angle sensor **411**, and the angular velocity ω_{m1} is output to the adder **601**.

Additionally, in the angular velocity calculator **561**, an angular velocity ω_{A1m} of the first arm **12** around the rotation axis **O1** is calculated on the basis of the frequency of the pulse signal input from the first angle sensor **411**, and the angular velocity ω_{A1m} is output to the subtractor **571**. In addition, the angular velocity ω_{A1m} is a value obtained by dividing the angular velocity ω_{m1} by a reduction ratio between the motor **401M** of the first drive source **401** and the first arm **12**, that is, in the joint **171**.

Additionally, the angular velocity of the first arm **12** around the rotation axis **O1** is detected by the first inertia sensor **31**. A detection signal of the first inertia sensor **31**, that is, an angular velocity ω_{A1} of the first arm **12** around the rotation axis **O1** detected by the first inertia sensor **31** is output to the subtractor **571**.

The angular velocity ω_{A1} and the angular velocity ω_{A1m} are input to the subtractor **571**, and the subtractor **571** outputs a value ω_{A1s} ($=\omega_{A1}-\omega_{A1m}$) obtained by subtracting the angular velocity ω_{A1m} from the angular velocity ω_{A1} to the converter **581**. The value ω_{A1s} is equivalent to a vibration component (vibration angular velocity) of the angular velocity of the first arm **12** around the rotation axis **O1**. Hereinafter, ω_{A1s} is referred to as a vibration angular velocity. In the present embodiment, feedback control is performed in which the vibration angular velocity ω_{A1s} (in detail, an angular velocity ω_{m1s} in the motor **401M** that is a value generated on the basis of the vibration angular velocity ω_{A1s}) is multiplied by a gain K_a to be described below and is returned to the input

side of the drive source **401**. Specifically, feedback control is performed on the drive source **401** so that the vibration angular velocity ω_{A1s} becomes as close to zero as possible. Accordingly, the vibration in the robot **1** can be suppressed. In addition, the angular velocity of the drive source **401** is controlled in the feedback control.

The converter **581** converts the vibration angular velocity ω_{A1s} into the angular velocity ω_{m1s} in the first drive source **401**, and outputs the angular velocity ω_{m1s} to the correction value calculator **591**. This conversion can be obtained by multiplying the vibration angular velocity ω_{A1s} by the reduction ratio between the motor **401M** of the first drive source **401** and the first arm **12**, that is, in the joint **171**.

The correction value calculator **591** multiplies the angular velocity ω_{m1s} by a gain (feedback gain) K_a that is a predetermined factor, obtains a correction value (first correction component) $K_a \cdot \omega_{m1s}$, and outputs the correction value $K_a \cdot \omega_{m1s}$ to the adder **601**.

The angular velocity ω_{m1} and the correction value $K_a \cdot \omega_{m1s}$ are input to the adder **601**. The adder **601** outputs an additional value of the angular velocity ω_{m1} and the correction value $K_a \cdot \omega_{m1s}$ to the subtractor **531** as the angular velocity feedback value ω_{fb} . In addition, the subsequent operation is as mentioned above.

As shown in FIG. 7, in addition to a position command P_c of the second drive source **402**, detection signals are input from the second angle sensor **412** and the second inertia sensor **32**, respectively, to the second drive source controller **202**. The second drive source controller **202** drives the second drive source **402** by feedback control using the respective detection signals so that a rotation angle (position feedback value P_{fb}) of the second drive source **402** calculated from the detection signal of the second angle sensor **412** becomes the position command P_c and an angular velocity feedback value ω_{fb} to be described below becomes an angular velocity command ω_c .

That is, the position command P_c is input to the subtractor **512** of the second drive source controller **202**, and the position feedback value P_{fb} to be described below is input from the rotation angle calculator **552**. In the rotation angle calculator **552**, the number of pulses input from the second angle sensor **412** is counted, and the rotation angle of the second drive source **402** according to the counted value is output to the subtractor **512** as the position feedback value P_{fb} . The subtractor **512** outputs a deviation (value obtained by subtracting the position feedback value P_{fb} from a targeted value of the rotation angle of the second drive source **402**) between the position command P_c and the position feedback value P_{fb} to the position controller **522**.

The position controller **522** performs predetermined calculation processing using the deviation input from the subtractor **512** and a proportional gain that is a predetermined factor, and calculates the targeted value of the angular velocity of the second drive source **402** according to the deviation. The position controller **522** outputs a signal showing the targeted value (command value) of the angular velocity of the second drive source **402** to the subtractor **532** as the angular velocity command (second angular velocity command) ω_c . In addition, in the present embodiment, a proportional control (P control) is performed as the feedback control. However, the feedback control is not limited to this.

The angular velocity command ω_c and the angular velocity feedback value ω_{fb} to be described below are input to the subtractor **532**. The subtractor **532** outputs a deviation (value obtained by subtracting the angular velocity feedback value ω_{fb} from the targeted value of the angular velocity of the second drive source **402**) between the angular velocity com-

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mand ω_c and the angular velocity feedback value ω_{fb} to the angular velocity controller 542.

The angular velocity controller 542 performs predetermined calculation processing including integration, using the deviation input from the subtractor 532, a proportional gain that is a predetermined factor, an integration gain, or the like, thereby generating a driving signal (driving current) of the second drive source 402 according to the deviation and supplying the driving signal to the motor 402M via the motor driver 302. In addition, in the present embodiment, the PI control is performed as the feedback control. However, the feedback control is not limited to this.

In this way, the feedback control is performed and the driving current of the second drive source 402 is controlled so that the position feedback value P_{fb} is as equal to the position command P_c as possible and the angular velocity feedback value ω_{fb} is as equal to the angular velocity command ω_c as possible. In addition, since the rotation axis O2 is orthogonal to the rotation axis O1, the rotation axis is not influenced by the operation or vibration of the first arm 12, and the operation of the second drive source 402 can be controlled independently from the first drive source 401.

Next, the angular velocity feedback value ω_{fb} in the second drive source controller 202 will be described.

In the angular velocity calculator 562, an angular velocity ω_{m2} of the second drive source 402 is calculated on the basis of the frequency of a pulse signal input from the second angle sensor 412, and the angular velocity ω_{m2} is output to the adder 602.

Additionally, in the angular velocity calculator 562, an angular velocity ω_{A2m} of the second arm 13 around the rotation axis O2 is calculated on the basis of the frequency of the pulse signal input from the second angle sensor 412, and the angular velocity ω_{A2m} is output to the subtractor 572. In addition, the angular velocity ω_{A2m} is a value obtained by dividing the angular velocity ω_{m2} by a reduction ratio between the motor 402M of the second drive source 402 and the second arm 13, that is, in the joint 172.

Additionally, the angular velocity of the second arm 13 around the rotation axis O2 is detected by the second inertia sensor 32. A detection signal of the second inertia sensor 32, that is, an angular velocity ω_{A2} of the second arm 13 around the rotation axis O2 detected by the second inertia sensor 32 is output to the subtractor 572. In addition, since the rotation axis O2 is orthogonal to the rotation axis O1, the angular velocity of the second arm 13 around the rotation axis O2 can be easily and reliably obtained without being influenced by the operation or vibration of the first arm 12.

The angular velocity ω_{A2} and the angular velocity ω_{A2m} are input to the subtractor 572, and the subtractor 572 outputs a value ω_{A2s} ($=\omega_{A2}-\omega_{A2m}$) obtained by subtracting the angular velocity ω_{A2m} from the angular velocity ω_{A2} to the converter 582. The value ω_{A2s} is equivalent to a vibration component (vibration angular velocity) of the angular velocity of the second arm 13 around the rotation axis O2. Hereinafter, ω_{A2s} is referred to as a vibration angular velocity. In the present embodiment, feedback control is performed in which the vibration angular velocity ω_{A2s} (in detail, an angular velocity ω_{m2s} in the motor 402M that is a value generated on the basis of the vibration angular velocity ω_{A2s}) is multiplied by a gain K_a to be described below and is returned to the input side of the second drive source 402. Specifically, feedback control is performed on the second drive source 402 so that the vibration angular velocity ω_{A2s} becomes as close to zero as possible. Accordingly, the vibration in the robot 1 can be suppressed. In addition, the angular velocity of the second drive source 402 is controlled in the feedback control.

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The converter 582 converts the vibration angular velocity ω_{A2s} into the angular velocity ω_{m2s} in the second drive source 402, and outputs the angular velocity ω_{m2s} to the correction value calculator 592. This conversion can be obtained by multiplying the vibration angular velocity ω_{A2s} by the reduction ratio between the motor 402M of the second drive source 402 and the second arm 13, that is, in the joint 172.

The correction value calculator 592 multiplies the angular velocity ω_{m2s} by a gain (feedback gain) K_a that is a predetermined factor, obtains a correction value (second correction component) $K_a \cdot \omega_{m2s}$, and outputs the correction value $K_a \cdot \omega_{m2s}$ to the adder 602. In addition, the gain K_a in the second drive source controller 202 and the gain K_a in the first drive source controller 201 may be the same or may be different.

The angular velocity ω_{m2} and the correction value $K_a \cdot \omega_{m2s}$ are input to the adder 602. The adder 602 outputs an additional value of the angular velocity ω_{m2} and the correction value $K_a \cdot \omega_{m2s}$ to the subtractor 532 as the angular velocity feedback value ω_{fb} . In addition, the subsequent operation is as mentioned above.

As shown in FIG. 8, in addition to a position command P_c of the third drive source 403, a detection signal is input from the third angle sensor 413 to the third drive source controller 203. The third drive source controller 203 drives the third drive source 403 by feedback control using the respective detection signals so that a rotation angle (position feedback value P_{fb}) of the third drive source 403 calculated from the detection signal of the third angle sensor 413 becomes the position command P_c and an angular velocity feedback value ω_{fb} to be described below becomes an angular velocity command ω_c .

That is, the position command P_c is input to the subtractor 513 of the third drive source controller 203, and the position feedback value P_{fb} to be described below is input from the rotation angle calculator 553. In the rotation angle calculator 553, the number of pulses input from the third angle sensor 413 is counted, and the rotation angle of the third drive source 403 according to the counted value is output to the subtractor 513 as the position feedback value P_{fb} . The subtractor 513 outputs a deviation (value obtained by subtracting the position feedback value P_{fb} from a targeted value of the rotation angle of the third drive source 403) between the position command P_c and the position feedback value P_{fb} to the position controller 523.

The position controller 523 performs predetermined calculation processing using the deviation input from the subtractor 512, a proportional gain that is a predetermined factor, and the like and calculates the targeted value of the angular velocity of the third drive source 403 according to the deviation. The position controller 522 outputs a signal showing the targeted value (command value) of the angular velocity of the third drive source 403 to the subtractor 533 as the angular velocity command ω_c . In addition, in the present embodiment, a proportional control (P control) is performed as the feedback control. However, the feedback control is not limited to this.

Additionally, in the angular velocity calculator 563, the angular velocity of the third drive source 403 is calculated on the basis of the frequency of a pulse signal input from the third angle sensor 413, and the angular velocity is output to the subtractor 533 as the angular velocity feedback value ω_{fb} .

The angular velocity command ω_c and the angular velocity feedback value ω_{fb} are input to the subtractor 533. The subtractor 533 outputs a deviation (value obtained by subtracting the angular velocity feedback value ω_{fb} from the targeted

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value of the angular velocity of the third drive source **403** between the angular velocity command ω_c and the angular velocity feedback value ω_{fb} to the angular velocity controller **543**.

The angular velocity controller **543** performs predetermined calculation processing including integration, using the deviation input from the subtractor **533**, a proportional gain that is a predetermined factor, an integration gain, or the like, thereby generating a driving signal (driving current) of the third drive source **403** according to the deviation and supplying the driving signal to the motor **403M** via the motor driver **303**. In addition, in the present embodiment, the PI control is performed as the feedback control. However, the feedback control is not limited to this.

In this way, the feedback control is performed and the driving current of the third drive source **403** is controlled so that the position feedback value P_{fb} is as equal to the position command P_c as possible and the angular velocity feedback value ω_{fb} is as equal to the angular velocity command ω_c as possible.

In addition, since the drive source controllers **204** to **206** are the same as the third drive source controller **203**, respectively, the description thereof is omitted.

As described above, according to the robot **1**, the vibration in the robot **1** can be easily and reliably suppressed.

First, in the control of the robot **1**, a huge calculation is unnecessary, and thereby, the response speed in the control of the robot **1** can be increased, and the configuration of the control device **20** can be simplified.

Additionally, in the control of the robot **1**, a calculation in which a singular point is present is unnecessary. Thus, the control of the robot **1** can be reliably performed, and thereby, vibration can be reliably suppressed.

Additionally, since the inertia sensors **31** and **32** are installed at the first arm **12** and the second arm **13**, respectively, and the first rotation axis $O1$ for the rotation of the first arm **12** and the second rotation axis $O2$ for the rotation of the second arm **13** are made orthogonal to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Hence, since control is performed by the calculation using these velocities, the vibration in the robot **1** can be more easily, accurately, and reliably suppressed.

In addition, since the first rotation axis $O1$ for the rotation of the first arm **12** and the second rotation axis $O2$ for the rotation of the second arm **13** are made orthogonal to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Since the rotational components with no mixture of these velocities are multiplied by feedback gains, respectively, the respective rotational components can be corrected with high precision.

Second Embodiment

FIG. **12** is a schematic view showing a second embodiment of a robot. FIG. **13** is a block diagram of portions of the robot shown in FIG. **12**.

In addition, in the following, for convenience of description, the upper side in FIG. **12** is referred to as "upper" and "upside" and the lower side is referred to as "lower" and "downside". Additionally, the base side in FIG. **12** is referred to as a "base end", and the opposite side is referred to as a "tip". Additionally, the rotation axes $O2$ and $O3$ are shown in an exaggerated manner in FIG. **12**, respectively. Additionally,

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inertia sensors **31**, **32**, and **33** are shown outside arms **12**, **13**, **14** in FIG. **12**, respectively, in order to clarify the presence of the sensors.

The second embodiment will be described below mainly regarding the differences from the aforementioned first embodiment, and the description of the same matters will be omitted.

As shown in FIG. **12**, in the robot **1** of the second embodiment, the third inertia sensor **33** is installed at the third arm **14**. The third inertia sensor **33** detects the angular velocity of the third arm **14** around the rotation axis $O2$. Although the installation position of the third inertia sensor **33** at the third arm **14** is not particularly limited, a tip portion of the third arm **14** is preferable. In the present embodiment, the third inertia sensor **33** is installed at the tip portion inside the third arm **14**. Since the vibration in the third arm **14** becomes the maximum at the tip portion of the third arm **14**, this can more reliably suppress the vibration in the robot **1**. In addition, it should be understood that the third inertia sensor **33** may be installed at a base end portion of the third arm **14**.

Additionally, the third inertia sensor **33** is not particularly limited, and in the present embodiment, for example, a gyroscope sensor, an acceleration sensor, or the like can be used.

In the robot **1**, in order to suppress the vibration in the first arm **12**, the second arm **13**, and the third arm **14**, the first inertia sensor **31**, the second inertia sensor **32**, and the third inertia sensor **33** are installed at all the first arm **12**, the second arm **13**, and the third arm **14** as mentioned above, and the operation of the first drive source **401**, the second drive source **402**, and the third drive source **403** is controlled on the basis of detection results of the first inertia sensor **31**, the second inertia sensor **32**, and the third inertia sensor **33**. Accordingly, the vibration in the first arm **12**, the second arm **13**, and the third arm **14** can be reliably suppressed, and thereby, the vibration in the entire robot **1** can be reliably suppressed.

Additionally, in the robot **1**, the third drive source controller **203** of the control device **20** is different from that of the first embodiment. The third drive source controller **203** will be described below.

As shown in FIG. **13**, the third drive source controller **203** has a subtractor **518**, a position controller **528**, a subtractor **538**, an angular velocity controller **548**, a rotation angle calculator **558**, an angular velocity calculator **568**, an adder-subtractor **618**, a converter **588**, a correction value calculator **598**, and an adder **608**. In addition to a position command P_c of the third drive source **403**, detection signals are input from the third angle sensor **413**, the second inertia sensor **32**, and the third inertia sensor **33**, respectively, to the third drive source controller **203**. The third drive source controller **203** drives the third drive source **403** by feedback control using the respective detection signals so that a rotation angle (position feedback value P_{fb}) of the third drive source **403** calculated from the detection signal of the third angle sensor **413** becomes the position command P_c and an angular velocity feedback value ω_{fb} to be described below becomes an angular velocity command ω_c .

That is, the position command P_c is input to the subtractor **518** of the third drive source controller **203**, and the position feedback value P_{fb} to be described below is input from the rotation angle calculator **558**. In the rotation angle calculator **558**, the number of pulses input from the third angle sensor **413** is counted, and the rotation angle of the third drive source **403** according to the counted value is output to the subtractor **518** as the position feedback value P_{fb} . The subtractor **518** outputs a deviation (value obtained by subtracting the position feedback value P_{fb} from a targeted value of the rotation

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angle of the third drive source 403) between the position command P_c and the position feedback value P_{fb} to the position controller 528.

The position controller 528 performs predetermined calculation processing using the deviation input from the subtractor 518, a proportional gain that is a predetermined factor, and the like and calculates the targeted value of the angular velocity of the third drive source 403 according to the deviation. The position controller 528 outputs a signal showing the targeted value (command value) of the angular velocity of the third drive source 403 to the subtractor 538 as the angular velocity command (third angular velocity command) ω_c . In addition, in the present embodiment, a proportional control (P control) is performed as the feedback control. However, the feedback control is not limited to this.

The angular velocity command ω_c and the angular velocity feedback value ω_{fb} to be described below are input to the subtractor 538. The subtractor 538 outputs a deviation (value obtained by subtracting the angular velocity feedback value ω_{fb} from the targeted value of the angular velocity of the third drive source 403) between the angular velocity command ω_c and the angular velocity feedback value ω_{fb} to the angular velocity controller 548.

The angular velocity controller 548 performs predetermined calculation processing including integration, using the deviation input from the subtractor 538, a proportional gain that is a predetermined factor, an integration gain, or the like, thereby generating a driving signal (driving current) of the third drive source 403 according to the deviation and supplying the driving signal to the motor of the third drive source 403 via the motor driver 303. In addition, in the present embodiment, the PI control is performed as the feedback control. However, the feedback control is not limited to this.

In this way, the feedback control is performed and the driving current of the third drive source 403 is controlled so that the position feedback value P_{fb} is as equal to the position command P_c as possible and the angular velocity feedback value ω_{fb} is as equal to the angular velocity command ω_c as possible. In addition, since the rotation axis O3 is orthogonal to the rotation axis O1, the rotation axis is not influenced by the operation or vibration of the first arm 12, and the operation of the third drive source 403 can be controlled independently from the first drive source 401.

Next, the angular velocity feedback value ω_{fb} in the third drive source controller 203 will be described.

In the angular velocity calculator 568, an angular velocity ω_{m3} of the third drive source 403 is calculated on the basis of the frequency of a pulse signal input from the third angle sensor 413, and the angular velocity ω_{m3} is output to the adder 608.

Additionally, in the angular velocity calculator 568, an angular velocity ω_{A3m} of the third arm 14 around the rotation axis O3 is calculated on the basis of the frequency of the pulse signal input from the third angle sensor 413, and the angular velocity ω_{A3m} is output to the adder-subtractor 618. In addition, the angular velocity ω_{A3m} is a value obtained by dividing the angular velocity ω_{m3} by a reduction ratio between the motor 403M of the third drive source 403 and the third arm 14, that is, in the joint 173.

Additionally, the angular velocity of the third arm 14 around the rotation axis O2 is detected by the third inertia sensor 33. A detection signal of the third inertia sensor 33, that is, an angular velocity ω_{A3} of the third arm 14 around the rotation axis O2 detected by the third inertia sensor 33 is output to the adder-subtractor 618. In addition, since the rotation axes O2 and O3 are orthogonal to the rotation axis O1, respectively, the angular velocity of the third arm 14

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around the rotation axis O2 can be easily and reliably obtained without being influenced by the operation or vibration of the first arm 12.

Additionally, the detection signal of the aforementioned second inertia sensor 32, that is, the angular velocity ω_{A2} of the second arm 13 around the rotation axis O2 detected by the second inertia sensor 32 is output to the adder-subtractor 618.

The angular velocity ω_{A3} , the angular velocity ω_{A2} , and the angular velocity ω_{A3m} are input to the adder-subtractor 618, and the adder-subtractor 618 outputs a value ω_{A3s} ($=\omega_{A3}-\omega_{A2}-\omega_{A3m}$) obtained by subtracting the angular velocity ω_{A2} and the angular velocity ω_{A3m} from the angular velocity ω_{A3} to the converter 588. The value ω_{A3s} is equivalent to a vibration component (vibration angular velocity) of the angular velocity of the third arm 14 around the rotation axis O3. Hereinafter, ω_{A3s} is referred to as a vibration angular velocity. In the present embodiment, feedback control is performed in which the vibration angular velocity ω_{A3s} (in detail, an angular velocity ω_{m3s} in the motor 403M that is a value generated on the basis of the vibration angular velocity ω_{A3s}) is multiplied by a gain K_a to be described below and is returned to the input side of the third drive source 403. Specifically, feedback control is performed on the third drive source 403 so that the vibration angular velocity ω_{A3s} becomes as close to zero as possible. Accordingly, the vibration in the robot 1 can be suppressed. In addition, the angular velocity of the third drive source 403 is controlled in the feedback control.

The converter 588 converts the vibration angular velocity ω_{A3s} into the angular velocity ω_{m3s} in the third drive source 403, and outputs the angular velocity ω_{m3s} to the correction value calculator 598. This conversion can be obtained by multiplying the vibration angular velocity ω_{A3s} by the reduction ratio between the motor 403M of the third drive source 403 and the third arm 14, that is, in the joint 173.

The correction value calculator 598 multiplies the angular velocity ω_{m3s} by a gain (feedback gain) K_a that is a predetermined factor, obtains a correction value (third correction component) $K_a \cdot \omega_{m3s}$, and outputs the correction value $K_a \cdot \omega_{m3s}$ to the adder 608. In addition, the gain K_a in the third drive source controller 203, the gain K_a in the first drive source controller 201, and the gain K_a in the second drive source controller 202 may be the same or may be different, respectively.

The angular velocity ω_{m3} and the correction value $K_a \cdot \omega_{m3s}$ are input to the adder 608. The adder 608 outputs an additional value of the angular velocity ω_{m3} and the correction value $K_a \cdot \omega_{m3s}$ to the subtractor 538 as the angular velocity feedback value ω_{fb} . In addition, the subsequent operation is the same as that of the first embodiment.

According to the robot 1, the same effects as the aforementioned first embodiment are obtained.

In this robot 1, since the control of suppressing vibration is also performed on the third arm 14, the vibration in the robot 1 can be more reliably suppressed.

Additionally, since the inertia sensors 31, 32, and 33 are installed at the first arm 12, the second arm 13, and the third arm 14, respectively, and the first rotation axis O1 for the rotation of the first arm 12 and the second rotation axis O2 for the rotation of the second arm 13 are made orthogonal to each other, the second rotation axis O2 for the rotation of the second arm 13 and the third rotation axis O3 for the rotation of the third arm 14 are made parallel to each other, the angular velocities of the respective arms can be detected as simple rotational components in which these velocities are not mixed. Hence, since control is performed by the calculation

using these velocities, the vibration in the robot 1 can be more easily, accurately, and reliably suppressed.

Third Embodiment

FIG. 14 is a block diagram showing portions of a third embodiment of a robot.

The third embodiment will be described below mainly regarding differences from the aforementioned second embodiment, and the description of the same matters will be omitted.

As shown in FIG. 14, in the robot 1 of the third embodiment, the second drive source controller 202 of the control device 20 is different from that of the second embodiment. The second drive source controller 202 will be described below.

As shown in FIG. 14, the second drive source controller 202 has an adder-subtractor 629 instead of the subtractor 577. In addition to a position command P_c of the second drive source 402, detection signals are input from the second angle sensor 412 and the third inertia sensor 33, respectively, to the second drive source controller 202. Additionally, an angular velocity ω_{A3m} of the third arm 14 around the rotation axis O3 is input from the third drive source controller 203 to the second drive source controller 202. The second drive source controller 202 drives the second drive source 402 by feedback control using the respective detection signals so that a rotation angle (position feedback value P_{fb}) of the second drive source 402 calculated from the detection signal of the second angle sensor 412 becomes the position command P_c and an angular velocity feedback value ω_{fb} to be described below becomes an angular velocity command ω_c .

That is, the position command P_c is input to the subtractor 519 of the second drive source controller 202, and the position feedback value P_{fb} to be described below is input from the rotation angle calculator 559. In the rotation angle calculator 559, the number of pulses input from the second angle sensor 412 is counted, and the rotation angle of the second drive source 402 according to the counted value is output to the subtractor 519 as the position feedback value P_{fb} . The subtractor 519 outputs a deviation (value obtained by subtracting the position feedback value P_{fb} from a targeted value of the rotation angle of the second drive source 402) between the position command P_c and the position feedback value P_{fb} to the position controller 529.

The position controller 529 performs predetermined calculation processing using the deviation input from the subtractor 519 and a proportional gain that is a predetermined factor, and calculates the targeted value of the angular velocity of the second drive source 402 according to the deviation. The position controller 529 outputs a signal showing the targeted value (command value) of the angular velocity of the second drive source 402 to the subtractor 539 as the angular velocity command (second angular velocity command) ω_c . In addition, in the present embodiment, a proportional control (P control) is performed as the feedback control. However, the feedback control is not limited to this.

The angular velocity command ω_c and the angular velocity feedback value ω_{fb} to be described below are input to the subtractor 539. The subtractor 539 outputs a deviation (value obtained by subtracting the angular velocity feedback value ω_{fb} from the targeted value of the angular velocity of the second drive source 402) between the angular velocity command ω_c and the angular velocity feedback value ω_{fb} to the angular velocity controller 549.

The angular velocity controller 549 performs predetermined calculation processing including integration, using the

deviation input from the subtractor 539, a proportional gain that is a predetermined factor, an integration gain, or the like, thereby generating a driving signal (driving current) of the second drive source 402 according to the deviation and supplying the driving signal to the motor 402M via the motor driver 302. In addition, in the present embodiment, the PI control is performed as the feedback control. However, the feedback control is not limited to this.

In this way, the feedback control is performed and the driving current of the second drive source 402 is controlled so that the position feedback value P_{fb} is as equal to the position command P_c as possible and the angular velocity feedback value ω_{fb} is as equal to the angular velocity command ω_c as possible.

Next, the angular velocity feedback value ω_{fb} in the second drive source controller 202 will be described.

In the angular velocity calculator 569, an angular velocity ω_{m2} of the second drive source 402 is calculated on the basis of the frequency of a pulse signal input from the second angle sensor 412, and the angular velocity ω_{m2} is output to the adder 609.

Additionally, in the angular velocity calculator 569, the angular velocity ω_{A2m} of the second arm 13 around the rotation axis O2 is calculated on the basis of the frequency of the pulse signal input from the second angle sensor 412, and the angular velocity ω_{A2m} is output to the adder-subtractor 629. In addition, the angular velocity ω_{A2m} is a value obtained by dividing the angular velocity ω_{m2} by a reduction ratio between the motor 402M of the second drive source 402 and the second arm 13, that is, in the joint 172.

Additionally, the angular velocity ω_{A3m} of the third arm 14 around the rotation axis O3 is output from the angular velocity calculator 5610 of the aforementioned third drive source controller 203 to the adder-subtractor 629.

Additionally, the detection signal of the aforementioned third inertia sensor 33, that is, the angular velocity ω_{A3} of the third arm 14 around the rotation axis O2 detected by the third inertia sensor 33 is output to the adder-subtractor 629 and an adder-subtractor 6110.

The angular velocity ω_{A3} , the angular velocity ω_{A2m} , and the angular velocity ω_{A3m} are input to the adder-subtractor 629, and the adder-subtractor 629 outputs a value ω_{A2s} ($=\omega_{A3}-\omega_{A2m}-\omega_{A3m}$) obtained by subtracting the angular velocity ω_{A2m} and the angular velocity ω_{A3m} from the angular velocity ω_{A3} to the converter 589. The value ω_{A2s} is equivalent to a vibration component (vibration angular velocity) of the total angular velocity of the second arm 13 and the third arm 14 around the rotation axis O2. Hereinafter, ω_{A2s} is referred to as a vibration angular velocity. In the present embodiment, feedback control is performed in which the vibration angular velocity ω_{A2s} (in detail, an angular velocity ω_{m2s} in the motor 402M that is a value generated on the basis of the vibration angular velocity ω_{A2s}) is multiplied by a gain K_a to be described below and is returned to the input side of the second drive source 402. Specifically, feedback control is performed on the second drive source 402 so that the vibration angular velocity ω_{A2s} becomes as close to zero as possible. Accordingly, the vibration in the robot 1 can be suppressed. In addition, the angular velocity of the second drive source 402 is controlled in the feedback control.

The converter 589 converts the vibration angular velocity ω_{A2s} into the angular velocity ω_{m2s} in the second drive source 402, and outputs the angular velocity ω_{m2s} to the correction value calculator 599. This conversion can be obtained by multiplying the vibration angular velocity ω_{A2s}

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by the reduction ratio between the motor **402M** of the second drive source **402** and the second arm **13**, that is, in the joint **172**.

The correction value calculator **599** multiplies the angular velocity $\omega m2s$ by a gain (feedback gain) Ka that is a predetermined factor, obtains a correction value (second correction component) $Ka \cdot \omega m2s$, and outputs the correction value $Ka \cdot \omega m2s$ to the adder **609**. In addition, the gain Ka in the second drive source controller **202**, the gain Ka in the first drive source controller **201**, and the gain Ka in the third drive source controller **203** may be the same or may be different, respectively.

The angular velocity $\omega m2$ and the correction value $Ka \cdot \omega m2s$ are input to the adder **609**. The adder **609** outputs an additional value of the angular velocity $\omega m2$ and the correction value $Ka \cdot \omega m2s$ to the subtractor **539** as the angular velocity feedback value ωfb . In addition, the subsequent operation is the same as the second embodiment.

According to the robot **1**, the same effects as the aforementioned second embodiment are obtained.

In the robot **1**, since the control of suppressing vibration is performed on the second drive source **402** that drives the second arm **13**, using the detection result of the third inertia sensor **33** installed at the third arm **14** on the tip side where a larger vibration than the second arm **13** is generated, the effect of suppressing the vibration in the robot **1** can be enhanced.

In detail, since the second drive source controller **202** performs the control of suppressing vibration on the second drive source **402** that controls the operation of the second drive source **402**, that is, rotates the second arm **13** by the angular velocities $\omega A3$, $\omega A2m$, and $\omega A3m$, using the detection result of the third inertia sensor **33** installed at the third arm **13** where a larger vibration than the second arm **13** is generated, the effect of suppressing the vibration can be enhanced.

Fourth Embodiment

FIG. **15** is a schematic view showing a fourth embodiment of a robot. FIG. **16** is a block diagram of portions of the robot shown in FIG. **15**.

In addition, in the following, for convenience of description, the upper side in FIG. **15** is referred to as “upper” and “upside” and the lower side is referred to as “lower” and “downside”. Additionally, the base side in FIG. **15** is referred to as a “base end”, and the opposite side is referred to as a “tip”. Additionally, the rotation axes **O2** and **O3** are shown in an exaggerated manner in FIG. **15**, respectively. Additionally, inertia sensors **31**, **32**, and **33** are shown outside arms **12**, **13**, **14** in FIG. **15**, respectively, in order to clarify the presence of the sensors.

The fourth embodiment will be described below mainly regarding differences from the aforementioned second and third embodiments, and the description of the same matters will be omitted.

The robot **1** of the fourth embodiment has an angle detection unit that detects an angle θ (hereinafter simply referred to as an “angle θ ”) formed between an axis (central axis) **131** of the second arm **13** and an axis **141** of the third arm **14** (to refer to FIG. **15**). In the present embodiment, the angle detection unit is constituted by the third angle sensor **413** and the control device **20**. That is, a rotation angle calculator **5512** of the third drive source controller **203** of the control device **20** counts the number of pulses input from the third angle sensor **413**, obtains the rotation angle of the third drive source **403** according to the counted value, and thereby, obtains the angle θ .

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Additionally, as shown in FIG. **16**, in the robot **1** of the fourth embodiment, the second drive source controller **202** of the control device **20** is different from that of the second embodiment and the third embodiment. The second drive source controller **202** will be described below.

As shown in FIG. **16**, the second drive source controller **202** has switches **63** and **64**. The switch **63** selects any one of an angular velocity $\omega A2$ and an angular velocity $\omega A3$, and outputs the selected angular velocity to an adder-subtractor **6211**. Additionally, the switch **64** switches between a case where an angular velocity $\omega A3m$ is output to the adder-subtractor **6211** and a case where the angular velocity $\omega A3m$ is not output to the adder-subtractor **6211**.

In the robot **1**, the second drive source controller **202** detects the angle θ using the third angle sensor **413** as mentioned above, and selects, according to the detected angle θ , a case where the switches **63** and **64** are switched so that the angular velocity $\omega A3$, an angular velocity $\omega A2m$, and the angular velocity $\omega A3m$ are input to the adder-subtractor **6211** and a case where the switches **63** and **64** are switched so that the angular velocity $\omega A2$ and the angular velocity $\omega A2m$ are input.

That is, when the angle θ is equal to or larger than a first threshold and equal to or smaller than a second threshold that is larger than the first threshold, the third arm **14** is in a state (hereinafter simply referred to as an “extended state” or an “extended posture”) where the third arm **14** is extended or slightly curved with respect to the second arm **13**. In this case, the second drive source controller **202** switches the switches **63** and **64** so that the angular velocity $\omega A3$, the angular velocity $\omega A2m$, and the angular velocity $\omega A3m$ are input to the adder-subtractor **6211**. In this case, the control of the second drive source **402** of the second drive source controller **202** is the same as that of the third embodiment.

Additionally, when the angle θ is smaller than the first threshold and larger than the second threshold, the third arm **14** is in a state (hereinafter simply referred to as a “folded state” or a “folded posture”) where the third arm **14** is largely curved with respect to the fourth arm **13**. In this case, the second drive source controller **202** switches the switches **63** and **64** so that the angular velocity $\omega A2$ and the angular velocity $\omega A2m$ are input to the adder-subtractor **6211**. In this case, the control of the second drive source **402** of the second drive source controller **202** is the same as that of the second embodiment.

Accordingly, the compatibility between enhancing the effect of suppressing vibration and the stability of control can be achieved.

That is, when the third arm **14** is in the extended posture, compared to the case of the folded posture, the control of the robot **1** is stable, but the inertia moment of the robot **1** is large and the vibration in the robot is large. Thus, the effect of suppressing vibration can be enhanced by controlling the second drive source **402** similar to the third embodiment, using a detection result of the third inertia sensor **33** installed at the third arm **14** on the tip side of the second arm **13** where a larger vibration than the second arm **13** is generated.

On the other hand, when the third arm **14** is in the folded posture, compared to the case of the extended posture, the inertia moment of the robot **1** is small and the vibration in the robot is small but control tends to become unstable and the robot **1** vibrates easily. Thus, the vibration in the robot **1** can be prevented and control can be stabilized by controlling the second drive source **402** similar to the second embodiment, using a detection result of the second inertia sensor **32**

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installed at the second arm **13** on the base end side of the third arm **14** where a smaller vibration than the third arm **14** is generated.

Here, although the first threshold is not particularly limited and is appropriately set according to terms and conditions, the first threshold is preferably set within a range of 45° to 135° and is more preferably set within a range of 70° to 110° . As one example, the first threshold is set to 90° , for example. Additionally, although the second threshold is not particularly limited and is appropriately set according to terms and conditions, the second threshold is preferably set within a range of 225° to 315° and is more preferably set within a range of 250° to 290° . As one example, the second threshold is set to 270° , for example. Accordingly, the compatibility of control can be more reliably achieved.

Hereinafter, an angular velocity feedback value ω_{fb} in the second drive source controller **202** will be specifically described.

In an angular velocity calculator **5611**, an angular velocity ω_{m2} of the second drive source **402** is calculated on the basis of the frequency of a pulse signal input from the second angle sensor **412**, and the angular velocity ω_{m2} is output to an adder **6011**.

Additionally, in the angular velocity calculator **5611**, the angular velocity ω_{A2m} of the second arm **13** around the rotation axis **O2** is calculated on the basis of the frequency of the pulse signal input from the second angle sensor **412**, and the angular velocity ω_{A2m} is output to the adder-subtractor **6211**. In addition, the angular velocity ω_{A2m} is a value obtained by dividing the angular velocity ω_{m2} by a reduction ratio between the motor **402M** of the second drive source **402** and the second arm **13**, that is, in the joint **172**.

When the angle θ is equal to or larger than the first threshold and is equal to or smaller than the second threshold, the angular velocity ω_{A3m} of the third arm **14** around the rotation axis **O3** is input from the angular velocity calculator **5612** of the aforementioned third drive source controller **203** to the adder-subtractor **6211**. Additionally, the detection signal of the aforementioned third inertia sensor **33**, that is, the angular velocity ω_{A3} of the third arm **14** around the rotation axis **O2** detected by the third inertia sensor **33** is input to the adder-subtractor **6211**.

The adder-subtractor **6211** outputs a value, which is obtained by subtracting the angular velocity ω_{A2m} and the angular velocity ω_{A3m} from the angular velocity ω_{A3} , to a converter **5811**. The value ω_{A2s} is equivalent to a vibration component (vibration angular velocity) of the total angular velocity of the second arm **13** and the third arm **14** around the rotation axis **O2**. Hereinafter, ω_{A2s} is referred to as a vibration angular velocity. In the present embodiment, feedback control is performed in which the vibration angular velocity ω_{A2s} (in detail, an angular velocity ω_{m2s} in the motor **402M** that is a value generated on the basis of the vibration angular velocity ω_{A2s}) is multiplied by a gain K_a to be described below and is returned to the input side of the second drive source **402**. Specifically, feedback control is performed on the second drive source **402** so that the vibration angular velocity ω_{A2s} becomes as close to zero as possible. Accordingly, the vibration in the robot **1** can be suppressed. In addition, the angular velocity of the second drive source **402** is controlled in the feedback control.

On the other hand, when the angle θ is smaller than the first threshold or larger than the second threshold, the angular velocity ω_{A3m} and the angular velocity ω_{A2} are not input to the adder-subtractor **6211**, and the detection signal of the aforementioned second inertia sensor **32**, that is, the angular

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velocity ω_{A2} of the second arm **13** around the rotation axis **O2** detected by the third inertia sensor **33** is input to the adder-subtractor **6211**.

The adder-subtractor **6211** outputs a value ω_{A2s} , which is obtained by subtracting the angular velocity ω_{A2m} from the angular velocity ω_{A2} , to the converter **5811**. The value ω_{A2s} is equivalent to a vibration component (vibration angular velocity) of the angular velocity of the second arm **13** around the rotation axis **O2**. Hereinafter, ω_{A2s} is referred to as a vibration angular velocity. In the present embodiment, feedback control is performed in which the vibration angular velocity ω_{A2s} (in detail, an angular velocity ω_{m2s} in the motor **402M** that is a value generated on the basis of the vibration angular velocity ω_{A2s}) is multiplied by a gain K_a to be described below and is returned to the input side of the second drive source **402**. Specifically, feedback control is performed on the second drive source **402** so that the vibration angular velocity ω_{A2s} becomes as close to zero as possible. Accordingly, the vibration in the robot **1** can be suppressed. In addition, the angular velocity of the second drive source **402** is controlled in the feedback control.

The converter **5811** converts the vibration angular velocity ω_{A2s} into the angular velocity ω_{m2s} in the second drive source **402**, and outputs the angular velocity ω_{m2s} to the correction value calculator **5911**. This conversion can be obtained by multiplying the vibration angular velocity ω_{A2s} by the reduction ratio between the motor **402M** of the second drive source **402** and the second arm **13**, that is, in the joint **172**.

The correction value calculator **5911** multiplies the angular velocity ω_{m2s} by a gain (feedback gain) K_a that is a predetermined factor, obtains a correction value (second correction component) $K_a \cdot \omega_{m2s}$, and outputs the correction value $K_a \cdot \omega_{m2s}$ to the adder **6011**. In addition, the gain K_a in the second drive source controller **202**, the gain K_a in the first drive source controller **201**, and the gain K_a in the third drive source controller **203** may be the same or may be different, respectively.

The angular velocity ω_{m2} and the correction value $K_a \cdot \omega_{m2s}$ are input to the adder **6011**. The adder **6011** outputs an additional value of the angular velocity ω_{m2} and the correction value $K_a \cdot \omega_{m2s}$ to the subtractor **5311** as the angular velocity feedback value ω_{fb} . In addition, the subsequent operation is the same as the second and third embodiments.

According to the robot **1**, the same effects as the aforementioned second and third embodiments are obtained.

In the robot **1**, suitable control can be performed according to the angle θ formed between the axis **131** of the second arm **13** and the axis **141** of the third arm **14**.

In addition, in the present embodiment, the configuration of the third drive source controller **203** is the same as that of the third drive source controller **203** of the second and third embodiments. However, the invention is not limited to this, and for example, the third drive source controller of the present embodiment is the same as that of the third drive source controller **203** of the first embodiment.

Although a robot has been described on the basis of the illustrated embodiments, the invention is not limited to this, and the configurations of the respective portions can be replaced with arbitrary configurations having the same functions. Additionally, other arbitrary structures may be added to the invention.

Additionally, the invention may be provided from the combinations of two or more arbitrary configurations (features) among the respective embodiments.

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In addition, the motors of the drive sources include, for example, stepping motors or the like in addition to the servo motors, respectively.

Additionally, in the above embodiments, as the angle sensors, other various sensors, such as encoders, resolvers, or potentiometers, which detect the rotation angle of rotor of the motors, may be used and various sensors, such as tachogenerators, which detect the rotating speed of the rotors of the motors, may be used. In addition, when the stepping motors are used as the motor, the rotation angle or rotating speed of the rotors of the motors may be detected, for example, by measuring the number of driving pulses input to the stepping motors.

Additionally, in the above embodiments, the gyroscope sensors can be used as the inertia sensors. However, the invention is not limited to these. For example, other various angular velocity sensors that detect the angular velocity of the arms may be used, and various acceleration sensors that detect the acceleration of the arms may be used. In addition, when the acceleration sensors are used, angular velocity is calculated using the detection values of the acceleration sensors.

Additionally, the types of the angle sensors and the respective inertia sensors are not particularly limited, and include, for example, an optical type, a magnetic type, an electromagnetic type, an electric type, or the like.

Additionally, in the above embodiments, the number of rotation axes of the robot is six. However, the invention is not limited to this, and the number of rotation axes of the robot may be two, three, four, five, or seven or more.

That is, in the above embodiments, the number of arms of the robot is six because the wrist has two arms. However, the invention is not limited to this, and the number of arms of the robot may be two, three, four, five, or seven or more.

Additionally, in the above embodiments, the robot is a single arm robot that has one arm coupling body obtained by rotatably coupling a plurality of arms. However, the invention is not limited to this. For example, as shown in FIG. 17, robots having a plurality of the arm coupling bodies, such as a

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double-arm robot 1A having the two arm coupling bodies 18 each obtained by rotatably coupling a plurality of arms, may be used.

What is claimed is:

1. A robot comprising:

- a base;
 - a first arm that is provided to the base and rotates around a first rotation axis;
 - a second arm that rotates around a second rotation axis in a direction intersecting a direction of the first rotation axis;
 - an inertia sensor that detects an angular velocity or acceleration of the first arm, and is provided on one of a first end or a second end of the first arm;
 - a drive source that rotates the first arm based on an output from the inertia sensor;
 - an angle sensor that detects a rotation angle of the first arm, wherein the drive source rotates the first arm based on an output from the angle sensor; and
 - a control unit of the drive source of the first arm that feeds back an angular velocity detected from the inertia sensor.
2. The robot according to claim 1, wherein the first rotation axis coincides with a normal line of an installation surface of the base.
3. The robot according to claim 1, wherein the inertia sensor is a gyroscope sensor.
4. The robot according to claim 1, wherein the drive source rotates the first arm based on a feedback gain.
5. The robot according to claim 1, wherein the inertia sensor is provided inside the first arm.
6. The robot according to claim 1, wherein a vibration of the first arm is suppressed based on an output from the inertia sensor.
7. The robot according to claim 1, wherein the inertia sensor is installed at a tip portion of the first arm.

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